14

DIETZGEN

TRADE MARK

ENGINEERS'

LEVEL BOOK

No. 410

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

| H | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | H |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 8.0 | 8.1 | 8.2 | 8.3 | 8.4 | 8.5 | 8.6 | 8.7 | 8.8 | 8.9 | 0 |
| 1 | 9.0 | 9.1 | 9.2 | 9.3 | 9.4 | 9.5 | 9.6 | 9.7 | 9.8 | 9.9 | 1 |
| 2 | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 2 |
| 3 | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 3 |
| 4 | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 4 |
| 5 | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 5 |
| 6 | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 6 |
| 7 | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 7 |
| 8 | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 8 |
| 9 | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 9 |
| 10 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 10 |
| 11 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 11 |
| 12 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 12 |
| 13 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 13 |
| 14 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 14 |
| 15 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 15 |
| 16 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 16 |
| 17 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 17 |
| 18 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 18 |
| 19 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 19 |
| 20 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 20 |
| 21 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 21 |
| 22 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 22 |
| 23 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 23 |
| 24 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 24 |
| 25 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 25 |
| 26 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 26 |
| 27 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 27 |
| 28 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 28 |
| 29 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 29 |
| 30 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 30 |
| 31 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 31 |
| 32 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 32 |
| 33 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 33 |
| 34 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 34 |
| 35 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 35 |
| 36 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 36 |
| 37 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 37 |
| 38 | 46.0 | 46.1 | 46.2 | 46.3 | 46.4 | 46.5 | 46.6 | 46.7 | 46.8 | 46.9 | 38 |
| 39 | 47.0 | 47.1 | 47.2 | 47.3 | 47.4 | 47.5 | 47.6 | 47.7 | 47.8 | 47.9 | 39 |
| 40 | 48.0 | 48.1 | 48.2 | 48.3 | 48.4 | 48.5 | 48.6 | 48.7 | 48.8 | 48.9 | 40 |

**Example**—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.





Book 14

| | |
|---|---|
| ? ? ? | 1 - B |
| Thompson Rd #7 Sec. F | 4 - |
| ? ? ? R.W. LEGGET'S | 12 - 13 |
| Mosley Rd. Sec. A-B-C OK 43 | |
| Alignment & Topo | 14 - 27 |
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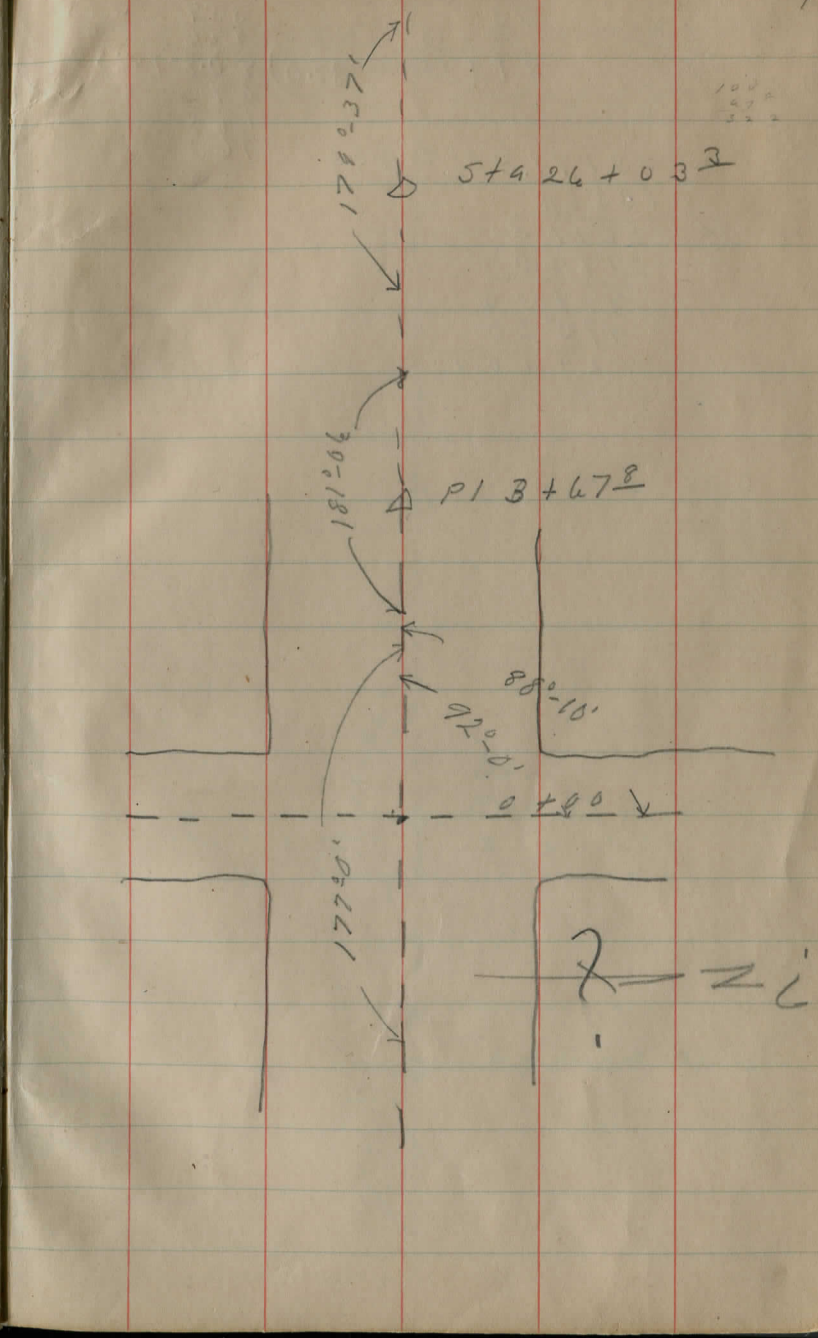
| B.M.'s | 72 |
| Ditch Between Thompson Center Road and Sidley Road | 44 - 55 |
| Sidley Road Sec. D-E T.14,58 | |
| Alignment & topo | 56 - 58 |
| Sections | 59 - 67 |
| San. Sewer Pope Home | 73 - 75 |

(14)


178°-37'
Sta 24+03
181°-04'
PI 3+67
85°-10'
92°-0'
0+80
177+0'

100
66
934

73
8+15
81+15

32.0)

225 ft
357
226
80.8 | 2.5
67
168
160

$280 | 1317.30 | 2.494
10560
26113
21120
49930
47520
24100

37+41.8 Sta 0+00 to
94+29.5 County Line
131+71.3 Total Length

2

Sta 73+87 L

Nail
Sta 56+06.6
12' > Stake

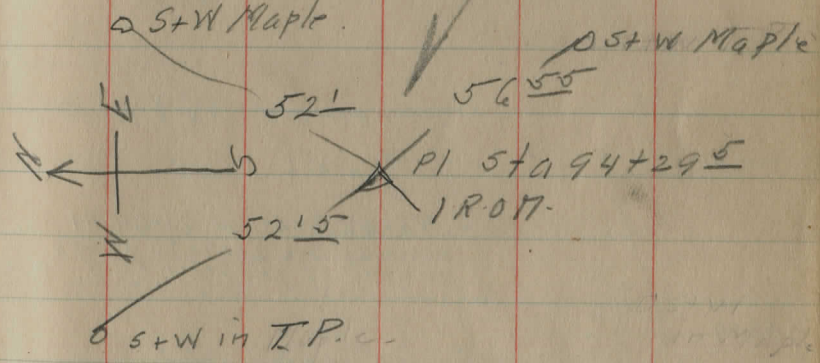
Stake < 12'

165.20'

179°-22'

Sta 39+93.7

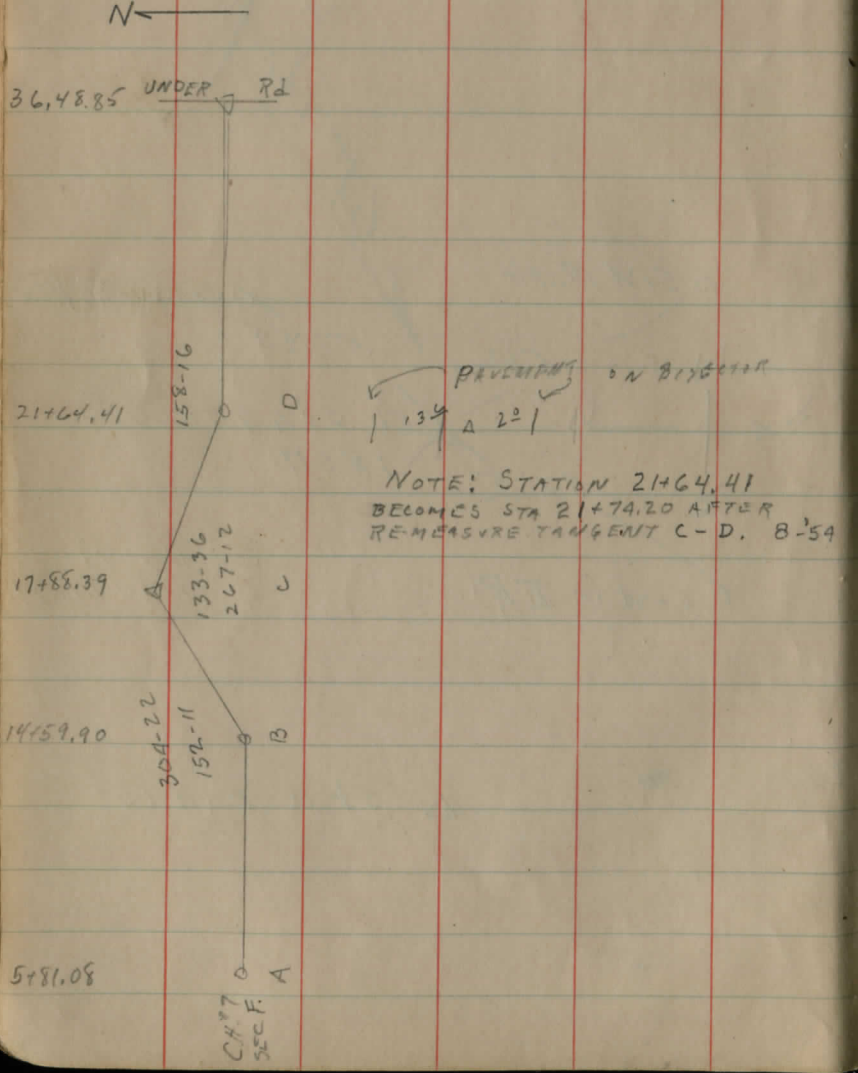
at Thompson Center




△ sta 81+15

Thompson Rd #7 Sec F
8/54 See Alignment Book 152 pg 52

START PROFILE & SEC. PAGE 7




4

GOING W FROM C

SET ON C BS. ON B ANGLES TO RT

| ANG | Cords on N. Edge Pave |
|---|---|
| 293-12 | POB 8.41 To N. Edge Pave = Bisector of "C" (S. Edge 26.8) |
| 0-0 | 24.70' |
| | 50' Cd = BEGIN 28' W of P.I. on TANGET C-B |
| 6-42 | |
| | 50 Cd |
| 4-16 | |
| | 50 Cd |
| 3-47 | |
| | 50 Cd |
| 1-59 | |
| | 50' Cd |
| 1-55 | |

SET ON B. BS on C ANGLES LT

| | |
|---|---|
| 85-15 | 50' Cd |
| 141-39 | 50 Cd |
| 146-44 | 50 Cd TANGENT WEST |

GOING EAST FROM C

SET IN C BS. ON D ANGLES LT

| | |
|---|---|
| 293-12 | POB 8.41 To Edge Pave = Bisector of "C" |
| 0-0 | 30 Cd |
| 3-45 | 50' |
| 3-07 | 50' |
| 2-04 | 50' |
| 1-44 | 50' |
| 1-25 | 50 |
| 1-22 | 50 |

| Ang | Chs | | | |
|---|---|---|---|---|
| 2-03 | 50 | | | |
| 3-30 | 50' | | | |
| 5-08 | 50' | | | |
| SET ON "D" | BS ON C | ANGLES TO RT | | |
| 156-03 | 50 | | | |
| 156-39 | 50 | ℄ = 6' S of N. Edg. Pavement | | |
| BLACK TOP SHELLS FROM 14 TO 18 EAST of Curve | | | | |
| | ANG D | | | |
| CONT'D BOTTOM PAGE 8 | + | H.I. | — | Elev |
| 17+0 | | | | |
| 17+50 | | | | |
| B.M. | 12.04 | 1263.91 ✓ | | 1251.87 |
| B.M. | | | 8.31 | 1251.87 ✓ |
| 18+0 | | | | |
| T.P. | 13.07 | 1260.18 ✓ | 0.22 | 1247.11 ✓ |
| 19+0 | | | | |
| T.P. | 11.34 | 1247.33 ✓ | 0.02 | 1235.99 ✓ |
| ±19+50 From Top Page 6 ↑ | | 1236.01 | | |

continue page 8

North ℄ South

1262.9 1.0 14' bottom ledge N. | 63.0 9.0 9.5 N. edge pave | 1263.2 0.70 | 63. 0.9 7.5' S. edge pave | 1262.4 1.5 14.5 bottom rock ledge S. | ±1276.4 Top rock + 14'

1257.5 6.4 2.5 N. edge pave | 1257.4 6.5 | 57.2 6.7 8' | 1256.0 7.9 14.5 S. edge pave. | 55.8 8.1 25' | 1255.9 8.0 31' base of ledge | 90° from line B.C

Vertical spk. w. root wild cherry 8' left ℄ 18+08

upper end fill wall N. side | 1252.7 7.5 13' | 1252.2 8.0 | 51.6 8.1 6' N. edge pave | 8.6 13' | 50.7 9.5 22.5 S. edge pave | 50.5 9.7 26.5' | 51.9 8.3 32.5 | 1248.9 11.8 36.5 boulder | 48.9 11.3 62.5

±18+70 Tele. pole 12.5' from ℄ 1235.6

Fall sharp to N. | 11.8 14' | 39.8 7.5 10' N. edge fill | 7.1 5.5' | 7.1 | 1240.2 7.5 9.5' ± upper end fill. SOUTH | 39.8 | 1239.8 7.5 25' | ± transition in alignment ℄ (Proposed) | 13' E of rock ledge

Hell hole down to N. 11.0 8.5 1227.5 | 1225.0 30' C.E.I.

To Bottom Page 5

| | + | HI | − | Elev |
|---|---|---|---|---|
| 20+0 | | | | |
| T.P. | 11.11 | 1236.01 ✓ | 0.81 | 1224.90 ✓ |
| 20+0 | | | | |
| | | | | |
| | | | | |
| 21+0 | | | | |
| T.P. | 11.41 | 1225.71 ✓ | 1.90 | 1214.30 ✓ |
| 21+65 culvert | | | | |
| | | | | |
| | | | | |
| 22+0 | | | | |
| | | | | |
| | | | | |
| 23+0 | | | | |
| | | | | |
| | | | | |
| 24+0 | | | | |
| T.P. | 11.40 | 1216.20 ✓ | 0.53 | 1204.80 ✓ |
| 24+82 | | | | |
| | | | | |
| | | | | |
| 25 | | | 6.9 | |
| T.P. | 12.41 | 1205.33 ✓ | 0.24 | 1192.92 ✓ |
| 26 | | | 1.1 | 1192.1 |

From Top Page 7 ↑

1193.16



North ℄ South

(O = occupation ℄)

1228.9 29.1 1222.5 29.4 29.6 1222.9
7.1 6.9 (6.5) 6.6 6.4 13.1 Flat out
10' 7' 9' 12.5' 21'
edge edge edge
stonewall (6.5) stonewall

1219.8 1222.2
down gradual 5.9 3.5
out 30' 16'
N. edge stone embank.

20+08 C.E.I. 18' from ℄

1215.6 16.6 15.3 18.5 1219.0 19.1 19.2 1219.7
bog for 10' then up 10.1 9.1 7.4 7.2 (6.7) 6.6 6.5 11.0 Fence 44'
30' 14.5' 11.0' 7.7' 6' 12.5' 30'
N edge S. edge

C.E.I. 21+45 30' N

1214.8 1211.3 14.7 14.5 1211.0
2.4 1213.8 1.4 4.9 1.5 (1.7) 1214.6 1.8 1.8 5.2 24' to Fence
30' 22.5 15.5' 12' 5' 1.6 3' 12' 12'
Top bank Tele. Pole Flowline N edge & culvert S. edge Top head wall outlet flowline

1213.3 1212.0 12.5 12.4 1212.8 12.5 12.6 1210.4
Flat N. 2.9 4.2 3.7 3.8 (3.4) 3.4 3.7 3.6 5.8
21' 17' 14' 10' 6.5' 10.5' 20'
N edge S. edge Fence & ditch Falls S.E.

1210.5 10.2 1207.8 09.2 1209.1 09.0 09.1 1207.9 1210.2
Flat N. 5.7 6.0 8.4 7.2 7.1 7.1 (7.0) 7.1 7.1 8.3 6.0 Fence 27.5
C.E.I. 26' 30' 18' 12' 8.5' 5.0' 11.5' 15' 18' 23' Tele. 23'S. 23+08
N. Edge S. edge

Miller drive 23+94

1207.2 1203.3 3.7 04.0 1204.3 04.2 4.7 1203.9 1207.5
Top bank 9.0 12.9 12.5 12.2 11.9 (11.8) 12.0 12.1 12.8 8.7 Iowa
Flat N. 18' 10.5' 8' 5.5' 12.5' 15.5' 19' 25.5' S.
N edge

1203.0 1198.7 09.5 1199.6
Top bank 2.3 6.6 5.8 5.7
Flat N. 18' 11' 7'

Kemeny Drive

1200.4 1198.4 1197.4 1202.9
4.9 6.9 6.9 (6.9) 7.0 7.3 7.9 2.4
30' 3-1 13' 15' 18.5' 30'
S. edge Top bank flat S.

| TO BOTTOM PAGE 6 | + | HI | − | ELV |
|---|---|---|---|---|
| 27 | | | 6.1 | 1187.1 |
| 27+60 | | | 8.9 | 1184.3 |
| B.M. | 5.16 | 1193.16 ✓ | 8-13-54 | 1188.00 |
| | 8-12-54 | | | |
| B.M. SET | | | 4.73 | 1188.00 ✓ |
| T.P. | 6.49 | 1192.73 ✓ | 1.72 | 1186.24 ✓ |
| 27 | | | 1.7 | 1186.3 |
| 28 | | | 6.2 | 1181.8 |
| 29 | | | 10.5 | 1177.5 |
| T.P. | 12.89 | 1187.96 ✓ | 0.0 | 1175.07 ✓ |
| 30 | | | 2.2 | 1172.9 |
| 31 | | | 5.9 | 1169.2 |
| 32 | | | 9.7 | 1165.4 |
| T.P. | 11.65 | 1175.07 ✓ | 0.0 | 1163.42 ✓ |
| 33 | | | 1.9 | 1161.5 |
| 34 | | | 7.3 | 1156.1 |
| 35 | | | 11.00 | 1152.4 |
| 35+48.85 | | | 12.1 | 1151.3 |
| 36+48.85 | | | 12.17 | 51.25 |
| BM. x 4 | 12.44 | 1163.42 ✓ | | 1150.98 ✓ |

↑ BEGIN

NOTE

↑ Profile & Cross Section on ℄ R-O-W & Corrected Stationing

Vertical spike N. root 20" maple 26' Rt A 27+60 (CORRECTED STATION ↙)

PROFILE OCCUPATION & MEASURED West from ℄ 42+7

↓

℄ ℄ CH. 7+42

X SW ℄ N. Hdwl in NW Quad #7 & Vanderkar Rd (CH. #42)

| | + | H.I | − | Elev |
|---|---|---|---|---|
| 17+0 | | | | |
| 16+50 | | | | |
| 16+0 | | | | |
| 15+50 | | | | |
| 8-18-54 BM. ↑ | 7.36 | 1285.19 ✓ | | 1277.83 |
| END ↓ | | | | |
| B.M. | | | 4.04 | 1277.83 ✓ |
| 15+15 | | | | |
| 15+50 | | | | |
| T.P. | 8.73 | 1281.87 ✓ | 1.02 | 1273.14 ✓ |
| 16+0 | | | | |
| 16+50 | | | | |
| T.P. FROM MIDDLE PAGE 5 ↑ | 10.90 | 1274.16 ✓ 1263.91 | 0.65 | 1263.26 ✓ |

N. ℄ 30' S. 40'

1278.9 6.8 — 1280.9 4.8

+.88 20" Cherry 28'

rock face ± 15' ← 1279.4 5.8 — 1279.9 5.3

1279.9 5.3 — 1280.0 5.2

30" oak at 30' 1279.0 6.2

EYE set in rock about 30' E of Hoeterle drive N. side Rd.

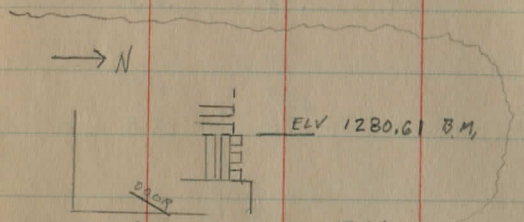
W. Point of rock outcrop on S. side ℄ level 4.1 — 15+23 = CEI POLE AT 23'

| 1277.7 | 15.2 | 75.9 | 1276.1 | 75.8 | 75.1 | 1278.9 |
|---|---|---|---|---|---|---|
| 4.2 | 6.7 | 6.0 | 5.8 | 6.1 | 6.8 | 3.0 |
| 15.5' | 13.5' | 7' | | 7.5 | 11' | 13' | 17 |
| Top rock W. end wall | ditch | N edge pave | | S. edge pave | | | Top bank |

| 73.2 | 1273.3 | 73.1 | 72.4 | 1280.4 |
|---|---|---|---|---|
| 1.6 | 0.9 | 0.9 | 1.1 | 1.8 | Top wall + 8" |
| 14' | 8-0' | 7' | 13' | 16+20 = |
| rock wall | N edge pave | S. edge pave | S. ditch and wall face | CEI AT 28' |

| 69.9 | 67.8 | 68.5 | 1268.6 | 68.1 | 67.9 | 1279.4 |
|---|---|---|---|---|---|---|
| 4.3 | 6.4 | 5.7 | 5.6 | 6.1 | 6.3 | Top wall + 11.5 |
| 19' | 15' | 9' | | 8' | 14' | |
| base rock wall | | N edge pave | | S. edge pave | base rock wall | |

| | + | HI | − | ELV |
|---|---|---|---|---|




C.EI. Communication Bldg Thompson Tnt Peak

| | | | | |
|---|---|---|---|---|
| B.M. set | | | 2.95 | 1280.61 |
| 13+50 | | | | |
| 14+0 | | | | |
| 15+0 | | | | |
| 15+15 | | | | |
| T.P. | 5.73 | 1283.56 | 9.36 | 1277.83 |
| B.M. set | | | 4.65 | 1280.54 |
| 17+30 | | | | |
| 17+41.50 | | | | |
| | | 1285.19 | | |



North ℄ South

Top third N.E. corner brick above concrete foundation

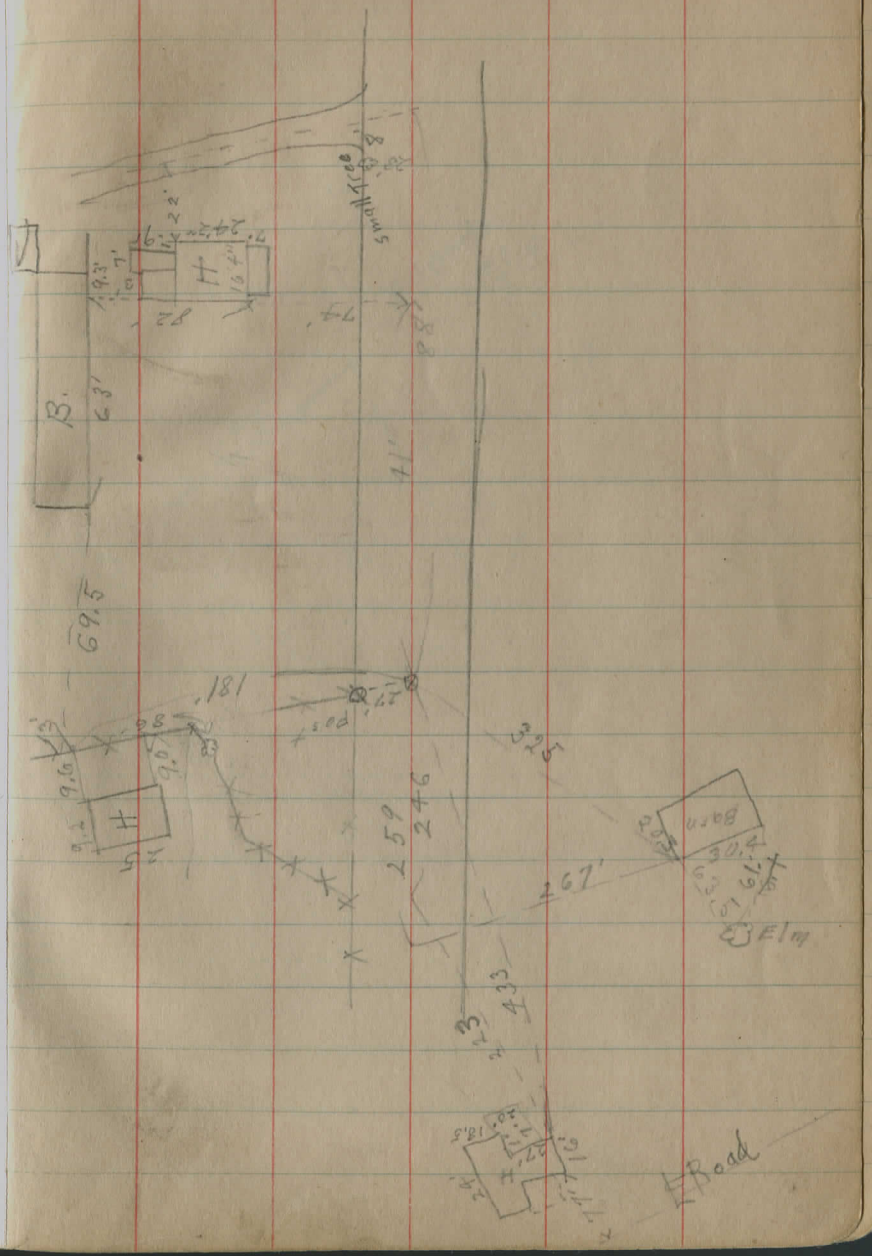
| | | | | | |
|---|---|---|---|---|---|
| | 71.8 | 72.1 | 1272.0 | 71.9 | |
| Flat out | 11.8 | 11.5 | 11.6 | 11.7 | Flat out |
| | 19' | 10' edge pave | | 6.5' edge pave | |
| | | 1273.1 | 1273.5 | 73.5 | |
| Flat out | | 10.5 | 10.1 | 10.1 | Flat out |
| | | 10' edge pave | | 5' edge pave | |
| | | 76.7 | 1277.0 | 77.0 | |
| Flat out | | 6.9 | 6.6 | 6.6 | Flat out |
| | | 10.8 edge pave | 1277.06 6.5 | 5.3 edge pave | |

39" Chestnut oak, sta 16+63, 40' S of ℄ vertical spike N root

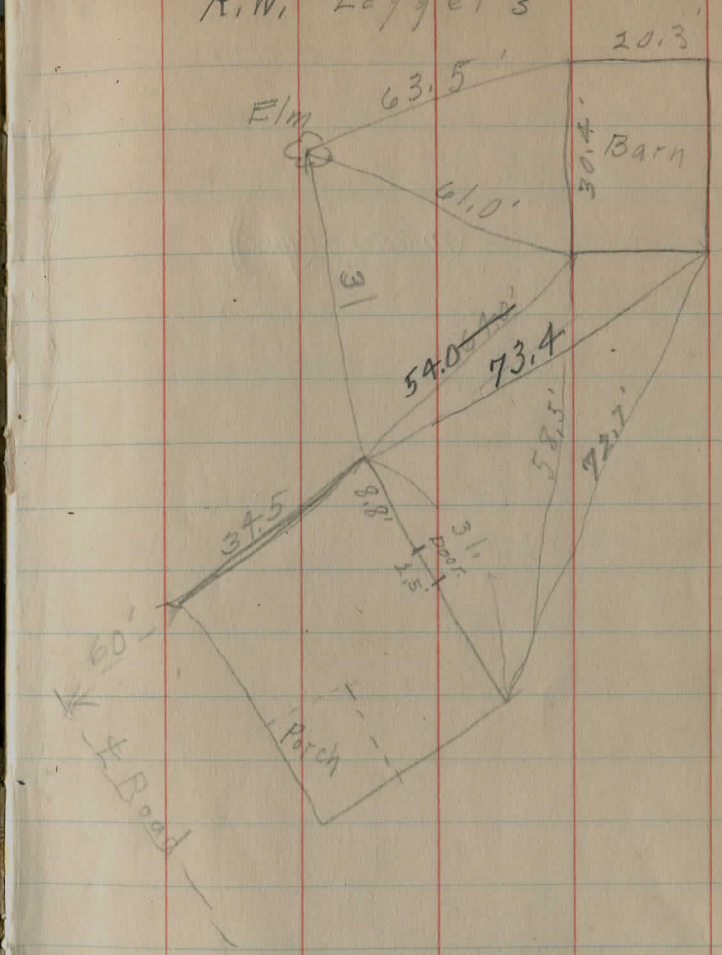
| | | | |
|---|---|---|---|
| 1275.0 | 77.3 | 78.6 | |
| 10.2 | 7.9 | 6.6 | |
| 18' rock point | 30' | 40' | |
| 1275.3 | 72.2 | 78.8 | |
| 9.9 | 8.0 | 6.4 | |
| 30' Top of rock | 40' | 46' | |

Nov. 30, 1925 Fiedler Marks





R. W. Leggett's


20.3'
63.5'
Elm
Barn
30.4'
61.0'
31'
54.0'
73.4'
58.5'
73.2'
34.5'
9.8'
31'
Back
25'
60'
Road
Porch

℄ Location Moseley Road

sidestakes set 25' Rt or on ℄

Sta 9+81.14 PI Def Rt 10°26' — Pipe Set

Curve Data

Δ = 10°26 (10-25-20 (7/48))

D = 6°

T = 87.18

E = 3.8

L = 173.89

PC = 8+93.96

PT = 10+67.85

Sta 0+00 Beginning of Imp. — Pipe Set

3/15/54 Runny Goodrich 14

Thompson Twp.

fd 6-87 fd 7/48 Box 87

9+50 Drive

19.01

36.26

88.50

Spk. N. side ÇE.I. 575164-X — good rot

NE ℄ Foundation

71.24 ~~71.79~~

H

Spk. S. root 24" Map. — ~~Sc W 15" Maple~~

3+15 Drive

S 60° E

32.30

Sc W 10" Maple

0+00 fd July '48

65°23' X

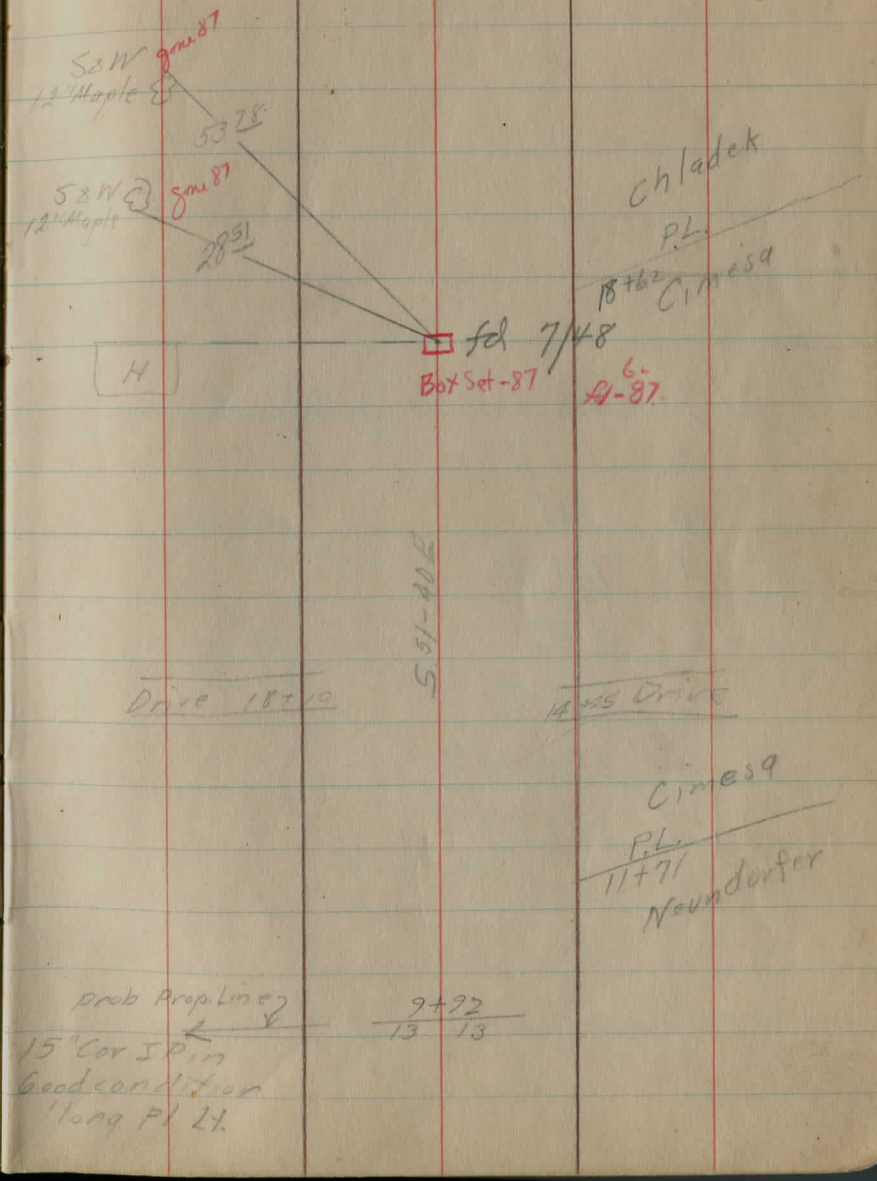
Box 87

Stacky

Geauga Co. Lake Co.

Sc W 18" Maple

Sta 18+62.65 POT Pipe Set



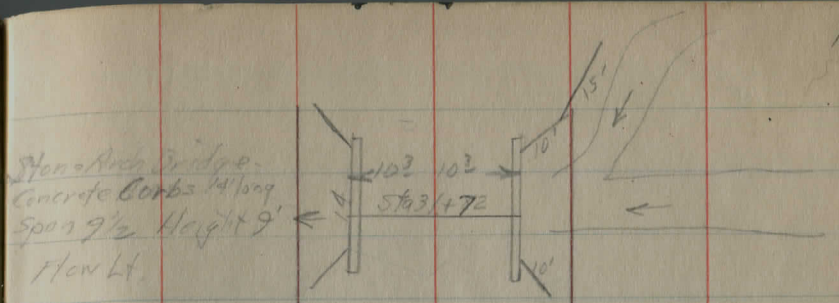
Sta 31+08.9 PI Dec Lt 63° 13' Proj Sta

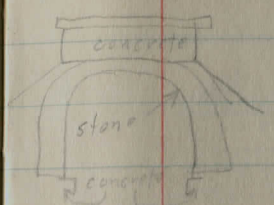
Curve Data
- Δ = 63°13'
- D = 22°
- T = 160.28
- E = 45.9
- L = 287.35
- PC = 29+47.79
- PT = 32+35.14
- R = 254.7

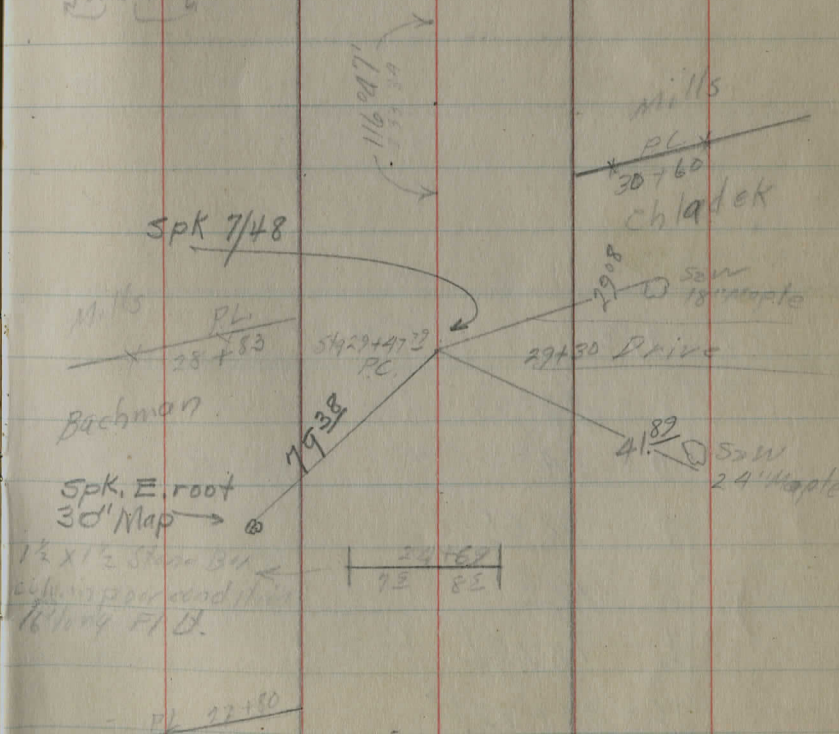
32+35.9 =
32+10 =
31+80
30+75 =
30+00 =
29+47.79 =

Sta 22 = End of Gravel

Stone Arch Bridge - Concrete Curbs 1st long. Span 9½ Height 9' How Lt.



Alley
19+00
61.98

35.52

Sta 35 + 61.98 POT Pipe Set

Sta 34 + 31.29 PI Dist Rt 44°53' Pipe Set

Curve Data

Δ = 44°53
D = 24°
T = 98.61
E = 19.6
L = 187.01
PC = 33+32.68
PT = 35+19.69
R = 233.9

35+19.69 = 0°00
35+00 = 2°24
34+00 = 14°24
33+32.68 = 22°26

Drive 35+40

35+50 Drive

Serv 20° Angle

37.30

Drive

46.78

Serv 12" Hole

224°53'

Eldridge Pk.

34+40

Mills

Remove 33+36 12'

3 x 3 Stone Box Culvert Ft. Lt

Sta 40+28.56 P.I. Def Rt 45°00' Pipe Set

Curve Data
- Δ = 45°00'
- D = 20°
- T = 118.67'
- E = 23.6
- L = 225.00
- PC = 39+09.89
- PT = 41+34.89
- R = 286.5

41+34.89 = 0°00
41+00 = 3°29
40+50 = 5°29
40+00 = 13°29
39+50 = 18°29
39+09.89 = 22°30

Sta 37+83.00 P.O.T. Pipe Found

1x1 Wood Box returned in fair condition F.I.R.

40+68 15 3

Drive 41+35

gone 5.2 W End 8" Apple

60.06

225.00

? NOT fd 6-87

39.75

S.2 W 15" Apple

Drive 39+60

Drive 38+80

Maanonen

PL 37+83

Mills

Box 87

Maanonen 37+75 PL

Eldridge

Sta 48+30.40 PI Pot L 59°20 P.I. Sta =

Δ = 59°20

D = 40°

T = 81.59

E = 21.6

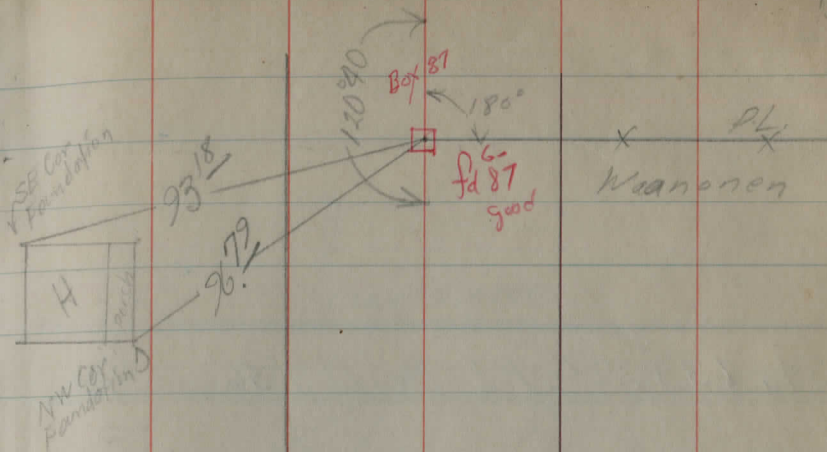
L = 148.33

PC = 47+48.81

PT = 48+97.14

R = 143.2

| | |
|---|---|
| 47+98.81 | = 0°00 |
| 48+75 | = 5°14 |
| 48+00 | = 10°14 |
| 48+25 | = 15°14 |
| 48+50 | = 20°14 |
| 48+75 | = 25°14 |
| 48+97.14 | = 29°40 |



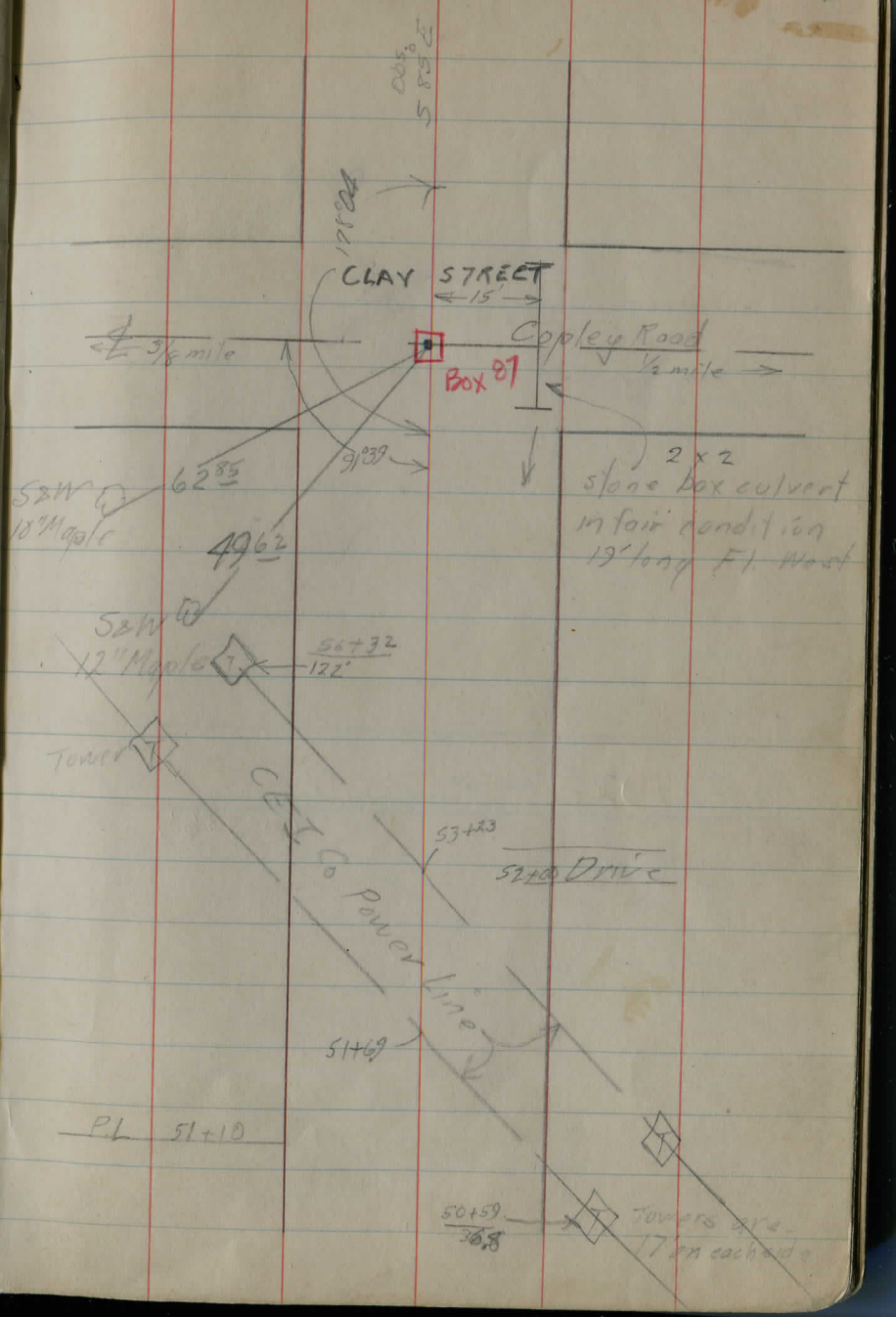

1½ x 1½ SE no Cor
extent in fair
condition FF Ck
distances are taken on
tangent

48+21
14 10

Drive 48+20

Approx P.I
46+55

Sta 63+20 $\frac{21}{}$ PI Def Lt 1°56' — Pipe Set



Sta 73+82.21 PI Def Rt 0°31' Pipe Set
(0°35½')

Van Santon
PL 80+23
Riley

76+20 PL
Riley

Drive 74+50

S&W
15" Maple

57.22

180°31

H ← 75'

Mon Box
89

S&W
15" Maple

52.00

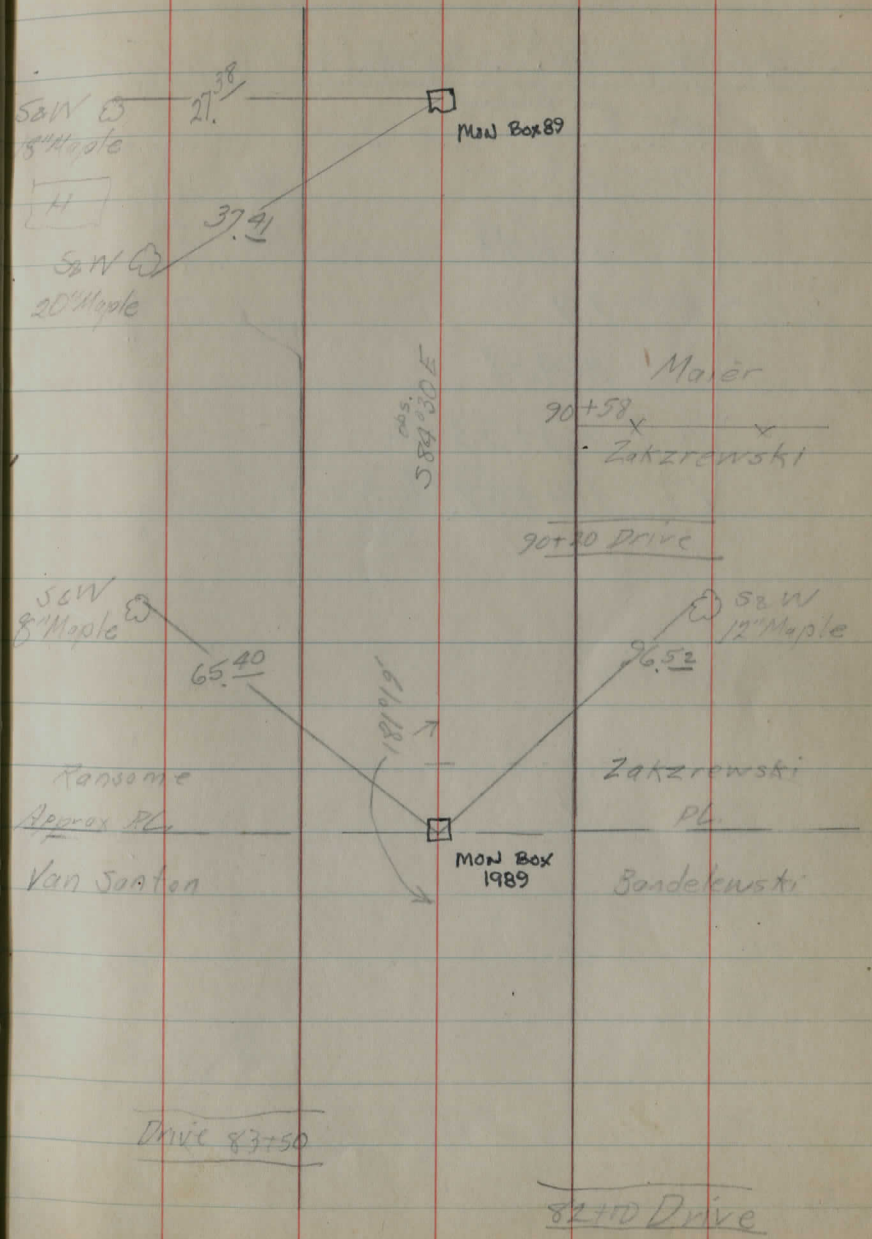
71+50 Drive

Plank Bridge Stone
About 4x12 Stringers
11'Span 3' Height

4E 11E
72+82

Sta 93+19.00 POT — Pipe Set

Sta 86+80.88 PI Det RT 119' — Pipe Set



Sta 104 + 36.84 PI Def Rt 8°11

Curve Data
- Δ = 8°11
- D = 4°
- T = 102.48
- E = 3.9
- L = 204.58
- PC = 103+33.36
- PT = 105+37.94

104 - 1.04

105 + 1.53

Tacked Hub
Yub
Kiehn
Tacked Hub
PL
10.00'
Sanford

40.62
99.51'
180°
25
Pipe Found
188°11
Mon Box 89

Bandelewski
40.00
Tacked Hub
PL.
Maier

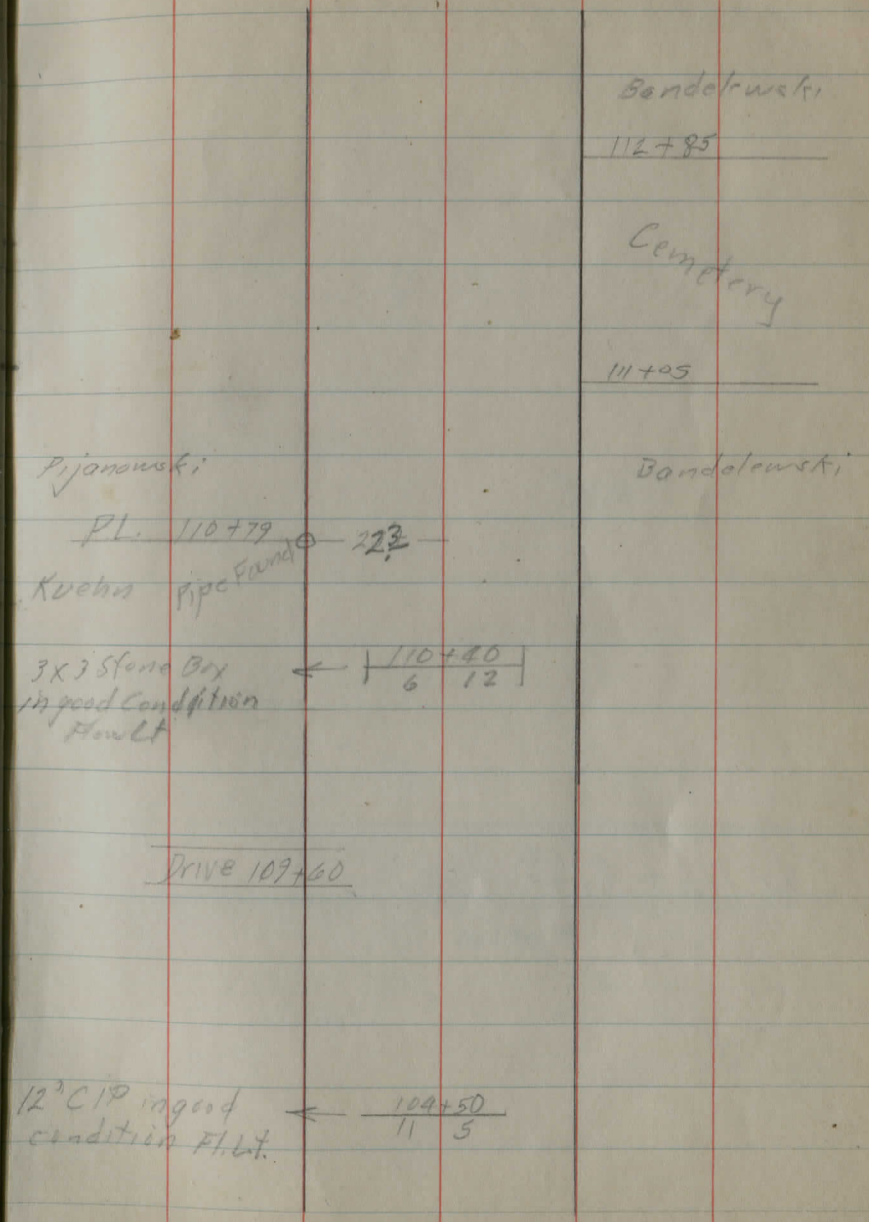
Drive 100+60

12" CIP & Wood Box culvert 16" CIP Flow Ln.
09+52
72.5
12.5

Sanford
PL. x 98+76 x Maier
Drive 78+65

98+76 Lane

Maier
PL. x 93+87 x Ransome
Drive 93+60


Bandelewski
112785
Cemetery
111+05
Bandelewski
Pijanowski
PL. 110+79
22?
Kvehn Pipe Fence
3x3 Stone Box in good Condition Howlt
110+40
6 12
Drive 109+60
12" CIP in good condition Fl. Lt.
104+50
11 5

Sta 116+81.62 OOT

Pipe Set

Crocker

PL 126+20

Bjamms Rt

CCrocker

126+20 PL

ACrocker

7x35 Stone Box Culvert
in fair condition
concrete slab
Flow Lt.

125+24
2 17

Dave 124+10

123+20 Dave

PL 120+85

1(x) Woodbury culvert
Flow Rt

117+36
7 11

DEWEY

(West Madison) Road

½ mile

¾ mile

Mon Box 88

9210

38.95

72.22

52W
15" Apple

S76°15'E

32W
15" Apple

Sta 127+44.69 PI Def Lt 8°09 Pipe Set.

Curve Data

Δ = 8°09' Lt

D = 7°

T = 58.31

E = 2.1

L = 116.43

PC = 126+86.29

PT = 128+02.72

127+.12

127+50 - 1.72

2x2 Stone Box culvert in fair condition Flt

Flows into 12" VSP

Northaccess field

131+62 / 10 / 10

68 W 18" Maple

71.70

30°

171.51

30.70 Pipe

132.56

52 W 6" Oak 3' Up.

2.76 miles

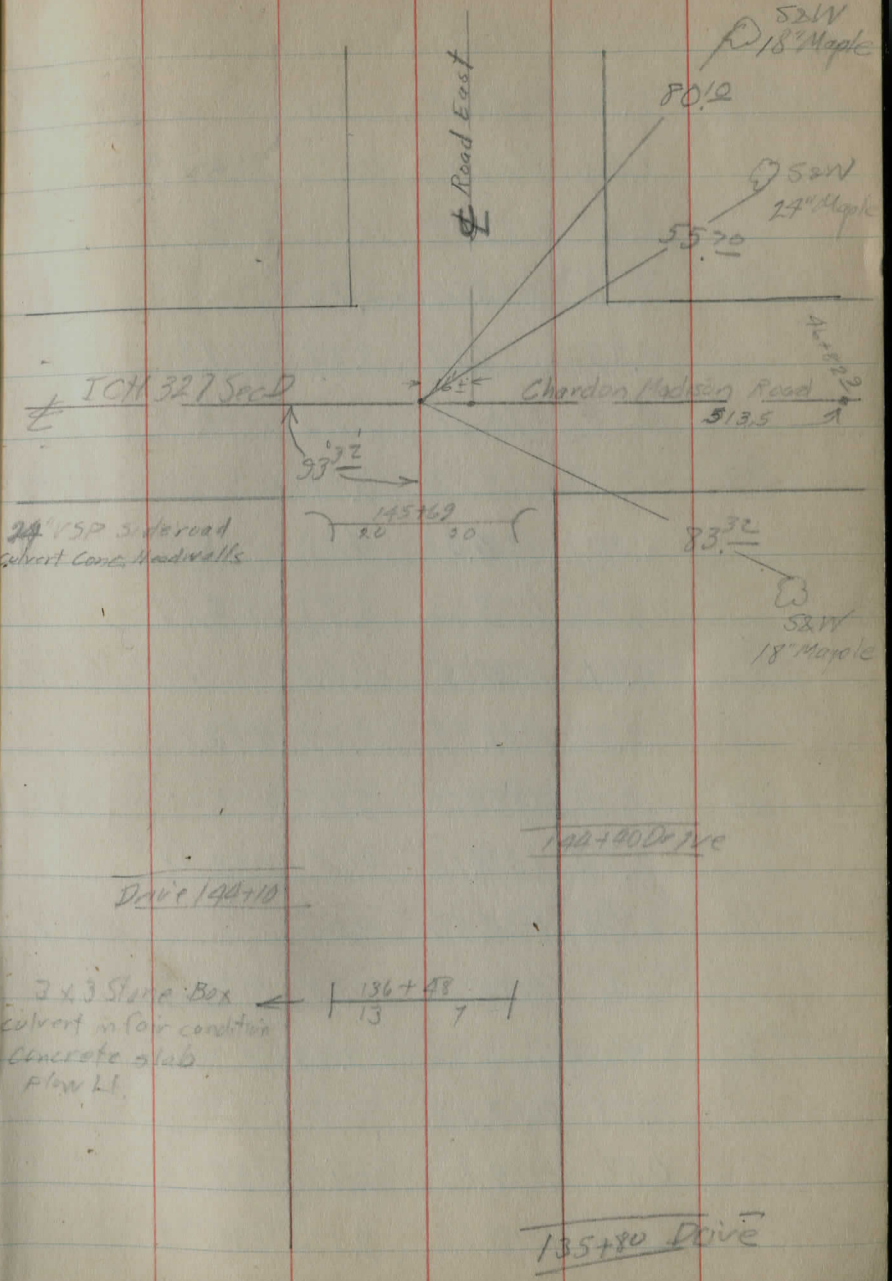
5280 | 14591
10 56
40310
36960
33500

Sta 145+91.20 End of Imp. Spike Set.

145+91.20 = Sta 51+94.8 ± of ICH 327-D Imp

145+81 = Edge of Pvt.





correct 1' Threaded

| | Bench Mark Levels | | | Hose Keyhead | |
|---|---|---|---|---|---|
| BM #15 | 0.75 | 1140.98 | | | 1140.23 |
| | 1.48 | 1131.70 | 10.76 | 1130.22 | |
| | 2.92 | 1123.15 | 11.47 | 1120.23 | |
| BM #14 | 2.23 | 1115.63 | 9.75 | | 1113.40 |
| | 4.53 | 1116.34 | 3.82 | 1111.81 | |
| | 4.00 | 1110.91 | 9.43 | 1106.91 | |
| BM #13 | | | 9.01 | | 1101.90 |
| | 2.30 | 1109.01 | 4.20 | 1106.71 | |
| | 1.22 | 1103.46 | 6.77 | 1102.24 | |
| BM #12 | 0.81 | 1094.58 | 9.69 | | 1093.77 |
| | 2.52 | 1091.28 | 5.82 | 1088.76 | |
| BM #11 | 2.00 | 1087.50 | 5.78 | | 1085.50 |
| | 5.34 | 1088.12 | 4.72 | 1082.78 | |
| BM #10 | 0.73 | 1084.30 | 4.55 | | 1083.57 |
| | 2.41 | 1076.03 | 10.68 | 1073.62 | |
| BM #9 | | | 2.39 | | 1066.64 |
| | 0.88 | 1067.52 | | | |
| | 0.56 | 1065.89 | 12.19 | 1055.33 | |
| | 1.48 | 1048.22 | 9.15 | 1046.74 | |
| | 36.10 | | 130.90 | | |

X SW Cor SR culvert Cohort Sta 145+68

Spike 5 Root 24" Maple 30' Lt ℄ Sta 136+60

Spike 5 Root 8" Elm 60 Lt ℄ Sta 125+60

Spike 5E Root 10" Elm Maple 25' Lt ℄ Sta 113+80

Top 30" Beech 35' Rt ℄ Sta 109+40

Spike 5 Root 12" Maple 25 Lt ℄ Sta 93+70

Spike 5 Root 10" Maple 25 Lt ℄ Sta 84+00
Entirely Tree in front of House

1412.3
36.1
1077.39
130.9
1414.9

| | | | | | |
|---|---|---|---|---|---|
| | | 1048.22 | | | |
| BM #8 | | | 2.94 | | 1045.28 |
| | 1.63 | 1042.12 | 7.73 | 1040.49 | check |
| | 2.85 | 1035.88 | 8.09 | 1033.03 | |
| BM #7 | 1.36 | 1030.51 | 6.43 | | 1029.15 |
| | 4.20 | 1026.66 | 9.35 | 1022.46 | |
| | 2.07 | 1020.18 | 7.55 | 1018.11 | |
| BM #6 | 5.99 | 1020.18 | 5.99 | | 1014.19 |
| | 3.63 | 1013.52 | 10.29 | 1009.89 | |
| | 2.01 | 1006.22 | 9.31 | 1004.21 | |
| | 0.48 | 1000.58 | 6.12 | 1000.10 | |
| BM #5 | 4.07 | 1000.58 | 4.07 | | 996.51 |
| | 0.97 | 993.71 | 7.84 | 992.74 | |
| | 0.11 | 981.79 | 12.03 | 981.68 | |
| | 8.72 | 987.56 | 2.95 | 978.84 | |
| | 11.34 | 998.54 | 0.36 | 987.20 | |
| BM #4 | | | 4.02 | | 994.52 |
| | 4.19 | 994.73 | 8.00 | 990.54 | |
| | 7.40 | 999.01 | 3.12 | 991.61 | |
| BM #3 | 3.26 | 998.79 | 3.48 | | 995.53 |

Spike S Wroot 18" Maple 25' Lt & Sta 73+80

Spike S Wroot 12" Maple 25' Lt & Sta 62+80
2.20 West of Corner

Top Hex. Nut 10' above ground NW Face N'ly & Tower 37' Rt & Sta 50+59

2 Vert spikes S root 15" Maple 25' Lt & Sta 38+20

Spike NE root 18" Maple 27' Rt & Sta 28+50

Spike W root 15" Maple 25' Lt & Sta 18+70

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 998.13 | | | | |
| | 3.26 | 993.84 | 8.21 | 990.58 | | |
| | 3.73 | 993.03 | 4.74 | 989.10 | | |
| BM #2 | | | 3.68 | | 989.35 | Spike NE root 15" Maple 28' Rt ℄ Sta 8+40 |
| | 1.83 | 987.11 | 7.75 | 985.28 | | |
| BM #1 | | | 6.21 | | 980.90 | Spike S Root 42" Oak 25' Lt ℄ Sta 0+00 |

# Profile Levels Moseley Road

| | | | | | |
|---|---|---|---|---|---|
| BM #1 | 5.84 | 98674 | | | 98070 |
| 0-200 | | | 11.5 | 75.2 | |
| 0-100 | | | 2.2 | 77.5 | |
| 0+00 | | | 75 | 79.2 | |
| 1 | | | 58 | 80.9 | |
| 2 | | | 4,4 | 823 | |
| 3 | | | 2.9 | 83.8 | |
| 4 | | | 1.7 | 85.0 | |
| | 7.53 | 99283 | 1.44 | 985.38 | |
| 5 | | | 6.2 | 86.6 | |
| 6 | | | 5.3 | 87.5 | |
| 7 | | | 4.5 | 88 3 | |
| 8 | | | 3.7 | 89.1 | |
| BM #2 | 3.45 | 99280 | 3.45 | 989.38 | 98935 |
| 9 | | | 3.6 | 89.2 | |
| | 5.19 | 99424 | 3.75 | 989.05 | |
| 9+92 | culvert | | 5.3 | 88.9 | |
| 10 | | | 5.3 | 88.9 | |
| 11 | | | 4.9 | 89.3 | |

Spike 5 Root 42" Oak 26' Lt & Sta 0+00

| 200 | Fl. | TO | TO | Fl |
|---|---|---|---|---|
| 8.3 | 7.4 | 5.9 | 5.6 | 7.1 |

Spike NE Root 15" Maple 28' Rt & Sta 8+98

| | | | | | | |
|---|---|---|---|---|---|---|
| 12 | | 999.24 | 4.6 | 89.6 | | |
| 13 | | | 4.1 | 90.1 | | |
| 14 | | | 3.2 | 91.0 | | |
| | 7.84 | 999.31 | 2.77 | 991.47 | | |
| 15 | | | 8.0 | 91.3 | | |
| 16 | | | 6.5 | 92.8 | | |
| 17 | | | 5.1 | 94.2 | | |
| 18 | | | 4.2 | 95.1 | | |
| BM #3 | 3.76 | 999.3 999.27 | 3.76 | 995.55 | 995.53 | Spike W Root 15" Maple 25' Lt & Sta 18+70 |
| 19 | | | 4.6 | 94.7 | | |
| 20 | | | 5.3 | 94.0 | | |
| | 2.36 | 995.42 | 6.23 | 993.06 | | |
| 21 | | | 2.4 | 93.0 | | |
| 22 | | | 3.6 | 91.8 | | |
| 23 | | | 4.8 | 90.6 | | |
| 24 | | | 5.5 | 89.9 | | |
| 24+69 | culvert | | 5.8 | 89.6 | | |
| | 6.35 | 996.55 | 5.22 | 990.20 | | |
| 25 | | | 6.9 | 89.6 | | |

200/2.8 100/8.4 Fl./8.5 TO/7.2 TO/7.4 Fl/7.7

| | | | | | |
|---|---|---|---|---|---|
| 26 | | 996 55 | 6.6 | ~~87.9~~ | |
| 27 | | | 55 | 91.0 | |
| 28 | | | 4.0 | 92.5 | |
| 34+9 | 2.04 | 996 56 (76.6) | 2.04 | 994 51 | 994.52 |
| 29 | | | 2.5 | 94.1 | |
| 30 | | | 5.5 | 91.1 | |
| | 0.33 | 987.31 | 9.58 | 976.78 | |
| 31 | | | 4.6 | 82.7 | |
| 31+50 | | | 9.9 | 77.4 | |
| 31+72 | Culvert | | 10.6 | 76.7 | |
| 32 | | | 10.9 | 76.4 | |
| 32+35 | | | 11.5 | 75.8 | |
| 32+50 | | | 13.2 | 74.1 | |
| 33 | | | 15.0 | 72.3 | |
| | 8.58 | 884.74 | 11.15 | 976.16 | |
| 33+32 | | | 14.0 | 70.7 | |
| 33+60 | | | 11.6 | 73.1 | |
| 34 | | | 7.6 | 77.1 | |
| 34+50 | | | 5.1 | 79.6 | |

Spike NE Root 18" Maple 27' Rt ± Sta 28+50

| FI | TO | TH | TH | TO | FI |
|---|---|---|---|---|---|
| 20.9 | 12.7 | 8.9 | 8.6 | 12.6 | 20.4 |

| | | | | | |
|---|---|---|---|---|---|
| 35 | | 884.74 | 0.01 | 84.7 | |
| | 11.86 | 995.21 | 1.39 | 883.35 | |
| 35+50 | | | 6.2 | 89.0 | |
| 36 | | | 4.4 | 70.8 | |
| 37 | | | 3.2 | 72.0 | |
| 38 | | | 1.6 | 73.6 | |
| | 7.29 | 1001.00 (01.0) | 1.50 | 993.71 | |
| B.M.=5 | 4.48 | 1000.99 | 4.48 | 996.52 | 996.51 |
| 39 | | | 6.1 | 94.9 | |
| 40 | | | 5.1 | 95.9 | |
| 40+68 | culvert | | | | |
| 41 | | | 3.6 | 97.4 | |
| 42 | | | 1.9 | 99.1 | |
| | 8.63 | 1007.71 | 1.91 | 999.08 | |
| 43 | | | 7.2 | 00.5 | |
| 44 | | | 5.8 | 01.9 | |
| 45 | | | 4.9 | 02.8 | |
| 46 | | | 3.6 | 04.1 | |
| 47 | | | 2.7 | 05.0 | |

2 Vert. Spikes Snoot 15" Maple 25' Lt. Sta 38+90

Fl. 7.9 Fl. 5.9

| | | | | | |
|---|---|---|---|---|---|
| | | 1007.71 | | | |
| 48 | | | 1.6 | 06.1 | |
| | 8.41 | 1015.37 | 0.75 | 1006.96 | |
| 48+21 | Culvert | | 9.1 | 06.3 | |
| 49 | | | 7.5 | 07.9 | |
| 50 | | | 5.2 | 10.2 | |
| BM 6 | 1.12 | 1015.51 | 1.12 | 1014.25 | 1014.39 |
| 51 | | | 3.6 | 11.9 | |
| 51+35 | 9.72 | 1023.23 | 2.00 | 1013.51 | |
| 52 | | | 6.4 | 16.8 | |
| 53 | | | 5.2 | 18.0 | |
| 54 | | | 3.8 | 19.4 | |
| 55 | | | 2.5 | 20.7 | |
| 56 | | | 1.9 | 21.3 | |
| | 7.24 | 1028.32 | 2.15 | 1021.08 | |
| 57 | | | 6.7 | 21.6 | |
| 58 | | | 6.1 | 22.2 | |
| 59 | | | 5.5 | 22.8 | |
| 60 | | | 4.1 | 24.2 | |
| 61 | | | 2.7 | 25.6 | |

| FI | TO | TO | FI |
|---|---|---|---|
| 11.0 | 9.5 | 10.3 | 12.3 |

Top Hex. nut 10" above Ground NW Face N.A. Tower 37' Rt ℄ Sta 58+59

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 1028.32 | | | | |
| | 10.44 | 1035.86 (36.7) | 2.90 | 1025.42 | | |
| 62 | | | 8.5 | 27.4 | | |
| BM #7 | 6.16 | 1035.61 | 6.16 | | 1029.45 | Spike 5' W R. of 12" Maple 25' L & Sta 62+80 |
| 63 | | | 6.9 | 28.7 | | |
| 63+21 | | | 6.6 | 29.0 | | |
| culvert 15' Rt. | | | 5.3 | 30.3 | | |
| 64 | | | 5.7 | 29.9 | | |
| 65 | | | 4.8 | 30.8 | | |
| 66 | | | 3.1 | 32.5 | | |
| | 8.37 | 1042.67 (42.7) | 1.31 | 1034.30 | | |
| 67 | | | 8.7 | 34.0 | | |
| 68 | | | 7.1 | 35.6 | | |
| 69 | | | 5.2 | 37.5 | | |
| 70 | | | 3.4 | 39.3 | | |
| 71 | | | 1.4 | 41.3 | | |
| | 7.67 | 1048.89 (48.9) | 1.45 | 1041.22 | | |
| 72 | | | 72 | 41.7 | | |
| 72+82 culvert | | | 55 | 43.4 | | |
| 73 | | | 5.6 | 43.3 | | |

| | | | | | |
|---|---|---|---|---|---|
| | 100/6.4 | | 100/4.9 | | |
| West | Fl. 7.9 | TO 6.3 | TO 6.3 | Fl 7.9 | East |
| | Fl 9.3 | | Fl 9.1 | | |

| | | | | | |
|---|---|---|---|---|---|
| | | 104859 | | | |
| 84+78 | 3.64 | 104892 | 3.64 | | 104528 Spike S Wroot 24" Maple 25' Lt & Sta 73+80 |
| 74 | | | 5.1 | 43.8 | |
| 75 | | | 3.5 | 45.4 | |
| 76 | | | 1.4 | 47.5 | |
| | 11.75 | 59.1 1059.08 | 1.59 | 104733 | |
| 77 | | | 9.6 | 49.5 | |
| 78 | | | 7.9 | 51.2 | |
| 79 | | | 6.3 | 52.8 | |
| 80 | | | 3.6 | 55.5 | |
| 81 | | | 1.1 | 58.0 | |
| | 10.91 | 69.5 1069.47 | 0.52 | 1058.56 | |
| 82 | | | 9.2 | 60.3 | |
| 83 | | | 6.9 | 62.6 | |
| 84 | | | 4.8 | 64.7 | |
| 84+97 | 2.81 | 1069.45 | 2.81 | | 106660 Spike S root 10" Maple 25' Lt & Sta 81+00 |
| 85 | | | 2.8 | 66.6 | |
| ~~86~~ | 11.54 | 1078.41 | 2.59 | 106.87 | |
| 86 | | | 9.7 | 68.7 | |
| 87 | | | 7.9 | 70.5 | |

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 1078.41 | | | | |
| 88 | | | 5.4 | 73.0 | | |
| 89 | | | 3.3 | 75.1 | | |
| 90 | | | 0.6 | 77.8 | | |
| | 9.12 | 86.0<br>1085.98 | 1.55 | 1076.86 | | |
| 91 | | | 6.6 | 79.4 | | |
| 92 | | | 5.7 | 80.3 | | |
| 93 | | | 5.0 | 81.8 | | |
| 31+10 | 2.40 | 1085.98 | 2.40 | 1083.58 | 1083.57 | Spike Snot+12" Maple 25'Lt & 5 to 93+70 |
| 94 | | | 3.5 | 82.5 | | |
| 95 | | | 2.6 | 83.4 | | |
| | 6.00 | 1088.41 | 3.57 | 1082.41 | | |
| 96 | | | 4.7 | 83.5 | | |
| 97 | | | 4.7 | 83.7 | | |
| 98 | | | 5.1 | 83.3 | | |
| 99 | | | 5.8 | 82.6 | | |
| 99+52 | culvert | | 5.8 | 82.6 | | |
| 100 | | | 6.0 | 82.4 | | |
| | 5.28 | 1087.20 | 5.79 | 1082.62 | | |
| 101 | | | 4.7 | 83.2 | | |

$\frac{\text{Fl.}}{8.2}$ $\frac{\text{Fl.}}{8.0}$

| | | | | | |
|---|---|---|---|---|---|
| | | 1087.70 | | | |
| 102 | | | 4.4 | 83.5 | |
| 103 | | | 4.2 | 83.7 | |
| 104 | | | 3.9 | 84.0 | |
| BM #11 | | | 2.40 | 1085.50 | 1085.50 |
| 104+50 | | | 3.9 | 84.0 | |
| | 5.27 | 1091.47 (71.5) | | | |
| 105 | | | 7.4 | 84.1 | |
| 106 | | | 7.0 | 84.5 | |
| 107 | | | 5.4 | 86.1 | |
| 108 | | | 4.5 | 87.0 | |
| 109 | | | 4.5 | 87.0 | |
| | 5.99 | 1074.74 | 2.72 | 1088.75 | |
| 110 | | | 6.9 | 87.8 | |
| 110+50 | culvert | | 6.8 | 87.9 | |
| 111 | | | 6.4 | 88.3 | |
| 112 | | | 6.9 | 87.8 | |
| 113 | | | 3.4 | 91.3 | |
| BM #12 | | | 1.50 | 1093.74 | 1093.77 |
| 114 | | | 0.7 | 94.0 | |
| | 9.59 | 1103.36 | | | |

Top 30" Boulder 35' Rt ℄ Sta 104+40

| Fl | To | To | Fl |
|---|---|---|---|
| 6.1 | 5.3 | 5.0 | 6.1 |

| Fl | To | To | Fl |
|---|---|---|---|
| 1.3 | 8.5 | 8.4 | 11.6 |

Spike SE Rot 10" Elm Maple 25' Lt ℄ Sta 113+80

| | | | | | |
|---|---|---|---|---|---|
| 115 | | 03.4 1103.36 | 58 | 97.6 | |
| 116 | | | 45 | 98.9 | |
| 116+81 | | | 3.0 | 00.4 | |
| 117 | | | 2.4 | 01.0 | |
| 117+36 | culvert | | 1.5 | 01.9 | |
| 118 | | | 1.3 | 02.1 | |
| | 795 | 12.6 1102.59 | 1.72 | 1101.64 | |
| 119 | | | 68 | 02.8 | |
| 120 | | | 5.9 | 03.7 | |
| 121 | | | 4.7 | 04.8 | |
| 122 | | | 3.6 | 06.0 | |
| 123 | | | 2.6 | 07.0 | |
| | 423 | 10.7 1110.67 | 3.15 | 1106.44 | |
| 124 | | | 3.2 | 07.5 | |
| 125 | | | 6.3 | 04.4 | |
| B.M. #13 | | | 8.78 | 1101.89 | 1101.90 |
| | 1179 | 13.7 1113.69 | | | |
| 125+24 | culvert | | 8.9 | 04.8 | |
| 126 | | | 8.9 | 04.8 | |

| | | | |
|---|---|---|---|
| 150 / 2.5 | | 150 / 1.8 | |
| Fl / 2.3 | TO / 1.5 | 1.2 TO / 1.2 | Fl / 2.2 |

Spike Snoot 8" Elm 60' Lt ℄ Sta 125+60

| | | | |
|---|---|---|---|
| Fl / 12.9 | TO / 10.3 | TO / 10.3 | Fl / 12.8 |

| | | | | | |
|---|---|---|---|---|---|
| | | 13.7<br>1113.69 | | | |
| 127 | | | 78 | 05.9 | |
| 128 | | | 2.5 | 11.2 | |
| 129 | | | 1.4 | 12.3 | |
| | 3.70 | 1115.53 | 1.86 | 1111.83 | |
| 130 | | | 4.8 | 10.7 | |
| 131 | | | 5.1 | 10.4 | |
| 131+62 | culvert | | 4.5 | 11.0 | |
| 132 | | | 4.8 | 10.7 | |
| 133 | | | 4.7 | 10.8 | |
| 134 | | | 4.2 | 11.3 | |
| | 8.42 | 19.9<br>1119.39 | 4.56 | 1110.97 | |
| 135 | | | 6.8 | 12.6 | |
| 136 | | | 6.3 | 13.1 | |
| 136+48 | | | 5.0 | 14.4 | |
| BM #14 | 5.95 | 1119.35 | 5.95 | | 1113.40 |
| 137 | | | 4.8 | 14.5 | |
| 138 | | | 3.7 | 15.6 | |
| | 11.70 | 27.4<br>1127.36 | 3.69 | 1115.66 | |
| 139 | | | 9.9 | 17.5 | |

| | | | |
|---|---|---|---|
| Fl / 8.0 | TO / 6.0 | TO / 6.0 | Fl / 7.8 |

| | | | |
|---|---|---|---|
| R / 8.3 | T.O. / 6.4 | TO / 6.2 | Fl / 9.2 |

Spike SE root 24" Maple 30' Lt ± 5' @ 136+60

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 27.4<br>1127.36 | | | | |
| 140 | | | 7.1 | 20.3 | | |
| 141 | | | 4.0 | 23.4 | | |
| 142 | | | 1.8 | 25.6 | | |
| | 1301 | 35.3<br>1158.28 | 2.09 | 1125.27 | | |
| 143 | | | 10.4 | 27.9 | | |
| 144 | | | 6.4 | 31.9 | | |
| 144+50 | | | 2.4 | 35.9 | | |
| 145 | | | 1.5 | 36.8 | | |
| | 7.53 | 1144.13 | 1.68 | 1136.60 | | |
| 145+69 | | | | | | |
| 145+91 | | | 4.8 | 39.3 | | |
| BM #15 | | | 3.92 | 1140.21 | 1140.23 | X cut S W Cor. South Headwall of Culvert Sta 145+69 |
| | 3.92 | 1144.15 | | | | |
| | 0.97 | 1132.76 | 12.36 | 1131.79 | | |
| BM #8 | | | 10.46 | 1122.30 | 1122.32 | Nail NE root 30" Maple 25' Lt & 600' N of Moseley Road |

$\frac{PI}{8.4}$ $\frac{PI}{6.7}$

$\frac{150}{9.2}$ $\frac{100}{0.6}$

Germany Corners Ditch
Northeast Thompson Ditch Location

Note: Sidestakes set 10' Lt. of West

Sta 8+00 Def Lt.

N 14° 45' E

0+34 Def. Rt.

N 9° 40' E

Sta 0+00 N end Bridge

482' N to ~~Sta 0+00~~ bridge from X rod
509' N to Sta 0+00 " X
314' N to 3+14 culv from X

3/6/35 Richey Merritt Rand 49

Relocated
See page 53

3+90± Interest

N. 9° 40' E.

0+00 ℄ stone

℄ County Highway No. 7 To Corner → 509'

Slab Top Bridge
Conc. Slab & wings
10' Span 18' long
5' high 10° skew

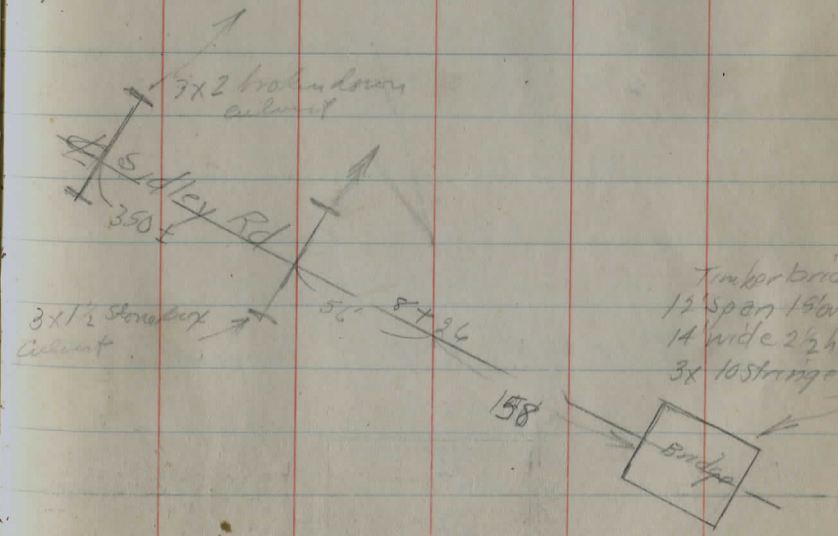
S 25 W ±

Sta 17+33 Def Rt

Sta 9 set at 15'

N 36° 30' E

Lateral 8+90±



Sta 20+00 end of Imp. Tangent for 1000' more

N65°E

Check levels for NE Thompson Ditch

| | | | | | |
|---|---|---|---|---|---|
| USGS BM | 3.98 | 1280.25 | | | 1276.27 |
| | 0.33 | 1275.15 | 5.43 | 1274.82 | |
| | 4.80 | 1269.39 | 10.56 | 1264.59 | |
| | 11.93 | 80.17 | 1.15 | 68.24 | |
| BM #2 | 2.62 | 80.17 | 2.62 | | 1277.55 |
| | 1.30 | 68.56 | 12.91 | 67.26 | |
| | 0.74 | 57.53 | 11.77 | 56.79 | |
| | 1.02 | 45.37 | 13.18 | 44.35 | |
| | 0.29 | 34.60 | 11.06 | 34.31 | |
| | 0.46 | 22.82 | 12.24 | 22.36 | |
| | 1.07 | 11.53 | 12.36 | 10.46 | |
| | 0.33 | 1199.69 | 12.17 | 1199.36 | |
| | 0.15 | 1188.26 | 11.56 | 1188.11 | |
| | 0.19 | 1177.05 | 11.40 | 1174.86 | |
| | 0.22 | 1165.22 | 12.05 | 1165.00 | |
| | 3.43 | 1156.93 | 11.92 | 1153.30 | |
| BM #3 | 5.95 | 1156.93 | 5.95 | 1150.98 | 1150.98 |
| | 1.01 | 151.06 | 6.88 | 1150.05 | |
| | 0.55 | 1138.81 | 12.80 | 38.26 | |
| | 4057 | | 16803 | | |

3/6/35

47

SW¼ Foundation Congregational Church.

X in Conc. Headwall Driveway Culv. N side at Top of Ledge

X in S.W. cor. N. Headwall at Under Ledge Rd.

| | | | | | | |
|---|---|---|---|---|---|---|
| | | 1138.81 | | | | |
| | 0.48 | 26.43 | 12.86 | 25.95 | | |
| | 0.52 | 14.96 | 11.99 | 14.44 | | |
| BM #4 | 0.64 | 1104.41 | 11.19 | | 1103.77 | X SW⅄ N Headwall culvert 100'E of Paus driveway |
| | 0.47 | 93.19 | 11.69 | 1092.72 | | |
| | 3.18 | 88.57 | 7.80 | 85.39 | | |
| | 1.17 | 79.86 | 9.88 | 78.69 | | |
| | 3.76 | 1070.31 | 13.31 | 66.55 | | |
| BM #5 | 1.97 | 66.61 | 5.67 | 1064.64 | | X E Headwall of driveway S side of Rd 150' W of Sta 0+00 |
| | 1.22 | 61.53 | 6.30 | 60.31 | | |
| | 0.89 | 54.31 | 8.11 | 53.42 | | |
| | 2.90 | 47.09 | 10.12 | 44.19 | | |
| BM #6 | | | 1.95 | | 1045.14 | X cut NW⅄ N Headwall Sta 0+00 |

# Germany Corners Ditch

## Cross Sections NE Thompson

| | | | | | |
|---|---|---|---|---|---|
| BM #1 | 1.35 | 1047.09 | | | 1045.74 |
| 0-200 | | | 8.4 | 38.7 | |
| 0-100 | | | 9.1 | 38.0 | |
| Flow S | | | 8.9 | 38.2 | |
| 0+00 | | | 9.3 | 37.8 | |
| 0+34 | | | 6.5 | 40.6 | |
| 1 | | | 7.8 | 39.3 | |
| 1+25 | | | 9.7 | 37.4 | |
| 1+50 | | | 7.0 | 40.1 | |
| | | | 7.3 | 39.8 | |
| 2 | 2.22 | 4280 | 6.51 | 104.58 | |
| 3 | | | 3.8 | 39.0 | |
| 4 | | | 4.8 | 38.0 | |
| 5 | | | 5.1 | 37.7 | |



Ditch

Xcut NE & N Headwall Sta 0+00

0 = sidestake Line or 10' Lt. of ℄

| | | | | |
|---|---|---|---|---|
| ℄ road 33 | TO 49 | | 6 8.3 | 15 98 |
| 0 63 | 9 63 | 13 87 | 22 92 | 25 71 |
| OC 0 | 0 87 | 7 78 | 16 68 | — |
| | 8 75 | 10 70 | 18 67 | 23 71 |
| OC 30 | 0 77 | 10 73 | 20 70 | 25 51 |
| OC 60 | 0 38 | 10 38 | 20 38 | |
| OC 60 | 0 48 | — | 20 48 | |
| | 0 51 | — | 20 51 | |

| | | | | | |
|---|---|---|---|---|---|
| | | 104280 | | | |
| 6 | | | 57 | 36.9 | |
| 7 | | | 63 | 36.5 | |
| | 3.36 | 16.8 104078 | 5.38 | 1037.42 | |
| 7+50 | | | 58 | 35.0 | |
| 8 | | | 50 | 35.8 | |
| 8+36 | | ℄ Road | 49 | 35.9 | |
| Bridge | | | | | |
| Culv, 50' North of 8+36 | | | | | |
| Culv, 250' North | | | | | |
| Road 175 N | | | 5.8 | 35.0 | |
| BM #2 | | | 4.35 | | 1036.36 |
| 9 | | | 4.8 | 36.0 | |
| 9+50 | same as 10 | | 6.1 | 34.7 | |
| 10 | | | 6.1 | 34.7 | |
| | 2.47 | 1037.56 | 5.69 | 1035.09 | |
| 11 | | | 6.8 | 30.8 | |



0 / 59 — 20

0 / 63 — 20

0 / 58 — 20

0 / 60 — 8 / 58 — 12 / 42 — 16 / 49 —

Floor 26 — Flow. E 5.3 1035.5

℄ 4.5 — Fl W — Fl E 6.8 1034.0

℄ 48 — Fl W — Fl E 2.8 1033.0

Spike SW root 30" Elm 20' Lt & Sta 8+90

OC / 0 — 0-5 / 90 — 0-2 / 80 — 7 / 70 — 9 / 48 — 20

OC / 50 — 0 / 58 — 5 / 54 — 10 / 61 — 20

OC / 10 — 0 / 33 — 10 / 38 — 15 / 42 —

| | | | | |
|---|---|---|---|---|
| | | 37.6 1037.56 | | |
| 17 | | | 50 | 32.6 |
| | | | | |
| 13 | | | 52 | 32.4 |
| 13+25 | | | 50 | 32.6 |
| 13+50 | | | 36 | 34.0 |
| 14 | | | 50 | 32.6 |
| 14+75 | | | 50 | 32.6 |
| 15 | | | 75 | 30.1 |
| | 3.89 | 34.3 1034.27 | 718 | 1030.38 |
| 15+50 | | | 3.9 | 38.4 |
| 16 | | | 4.1 | 30.2 |
| | | | | |
| 17 | | | 4.9 | 29.4 |
| | | | | |
| 17+33 | | | 56 | 28.7 |
| 17+60 | | | 52 | 29.1 |
| 18 | | | 50 | 29.3 |
| 18+25 | | | 79 | 26.4 |
| 18+40 | | | 66 | 27.7 |

OC/50 0/30 -20 —

OC/40 0/52 -20 —

0/49 20/55

OC/10 0/70 10/75 13/92 -20 —

OC/5 0/45 5/41 -20 — —

OC/0 0/60 8/60 10/49 -20

X at +75 0/56 -12 14/69 -20 22/45 -

OC/1475 0/50 -20

| | | | | | |
|---|---|---|---|---|---|
| | | 103427 | | | |
| 19 | | | 8.7 | 25,6 | |
| 19+25 | channel | | 10,6 | 23.7 | |
| 20 | | | 87 | 25.6 | |
| 21 | Flow | | 12.1 | 22.2 | |
| 22 | Flow | | 13.7 | 21.1 | |
| BM #3 | | | 5.43 | | 102884 |

OC
Ø15'

0 - 20
87

X at 19+25

0 / 85 — 10 / 87 — 20 / 104 — Ø17 / 23 / 11.1

Spike SE root 30" Beech 75' Lt & Sta 184 75

check Level

| | | | | | |
|---|---|---|---|---|---|
| BM #3 | 5.43 | 103427 | | 102884 | |
| | 8.08 | 1039.59 | 2.76 | 1031.51 | |
| | 6.40 | 104033 | 5.66 | 103393 | |
| BM #2 | | | 3.89 | 103644 | 103613 |
| | 5.45 | 104334 | 2.49 | 103789 | |
| | 4.84 | 104632 | 1.86 | 104148 | |
| BM #1 | | | 1.19 | 104513 | 104514 ✓ |

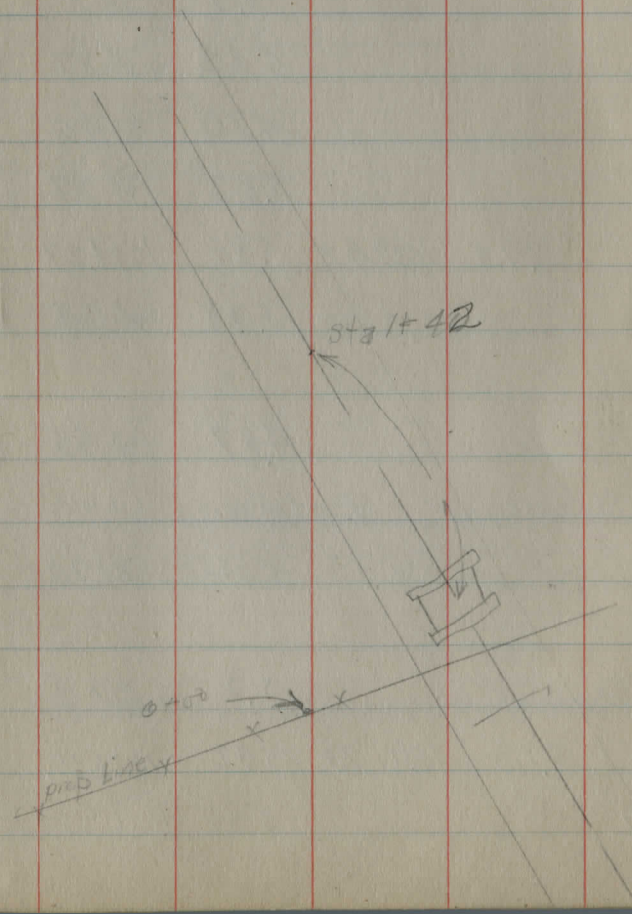
5/14/35 Richey Pond Grau

Germany Corners Ditch Relocation
Sidestakes set 10' Lt.
Sta 6+50 End of Imp.

Sta 1+71 Def. Lt. 5°43'

N 40 E

Sta 0+00 Beginning of Imp.



X Sections on Relocation

| | | | | | |
|---|---|---|---|---|---|
| 3+42 | 3.74 | 1040.10 | | | 1036.36 |
| 0 | | | 2.99 | 37.11 | |
| Flow Bridge W | | | 6.0 | 34.1 | |
| " E | | | 5.6 | 34.5 | |
| 1 | | | 4.46 | 35.64 | |
| 1+42 | | | 3.3 | 36.8 | |
| 2 | | | 5.23 | 34.87 | |
| 3 | | | 4.70 | 35.40 | |
| 4 | | | 5.83 | 34.27 | |
| | 3.15 | 1087.42 | 5.83 | 1034.27 | |
| 5 | | | 3.38 | 34.04 | |
| 6 | | | 4.87 | 32.55 | |
| Sta Old = 6+80 New | | End of Jap | 6+50 | | |
| 7 | | | 5.52 | 31.90 | |
| 8 channel | | | 8.2 ch. | 27.2 | |
| | 3.73 | 1039.73 | 1.42 | 1036.00 | |
| BM #2 | | | 3.38 | 1036.35 | 1036.36 |

34.5

| | | | | | |
|---|---|---|---|---|---|
| 0 | 6 | 12 | 16 | 20 | — |
| 32 | 7.8 | 3.6 | | 3.9 | |

35.5

| | | | | | |
|---|---|---|---|---|---|
| 0 | 19 | 23 | — | — | — |
| 45 | 46 | 30 | | | |

34.0

| | | | | | |
|---|---|---|---|---|---|
| 0 | 6 | 14 | 23 | — | — |
| 3 | 52 | 61 | 43 | | |

| | | |
|---|---|---|
| 0 | 22 | 35.3 |
| 48 | 48 | |

| | | |
|---|---|---|
| 0 | 20 | 34.2 |
| 57 | 69 | |

33.5

| | | | | |
|---|---|---|---|---|
| 0 | 11 | 23 | — | — |
| 35 | 39 | 42 | | |

32.5

| | | | | |
|---|---|---|---|---|
| 0 | 15 | 23 | 28 | — |
| 50 | 49 | 69 | | |

31.1

| | | | | | |
|---|---|---|---|---|---|
| 0 | 8 | 14 | 17 | 21 | 25 |
| 53 | 55 | 63 | 72 | | 55 |

Bridge - Stone Abutments

N - 28'  S - 18'

Floor 2x9 x 14  15 lodg

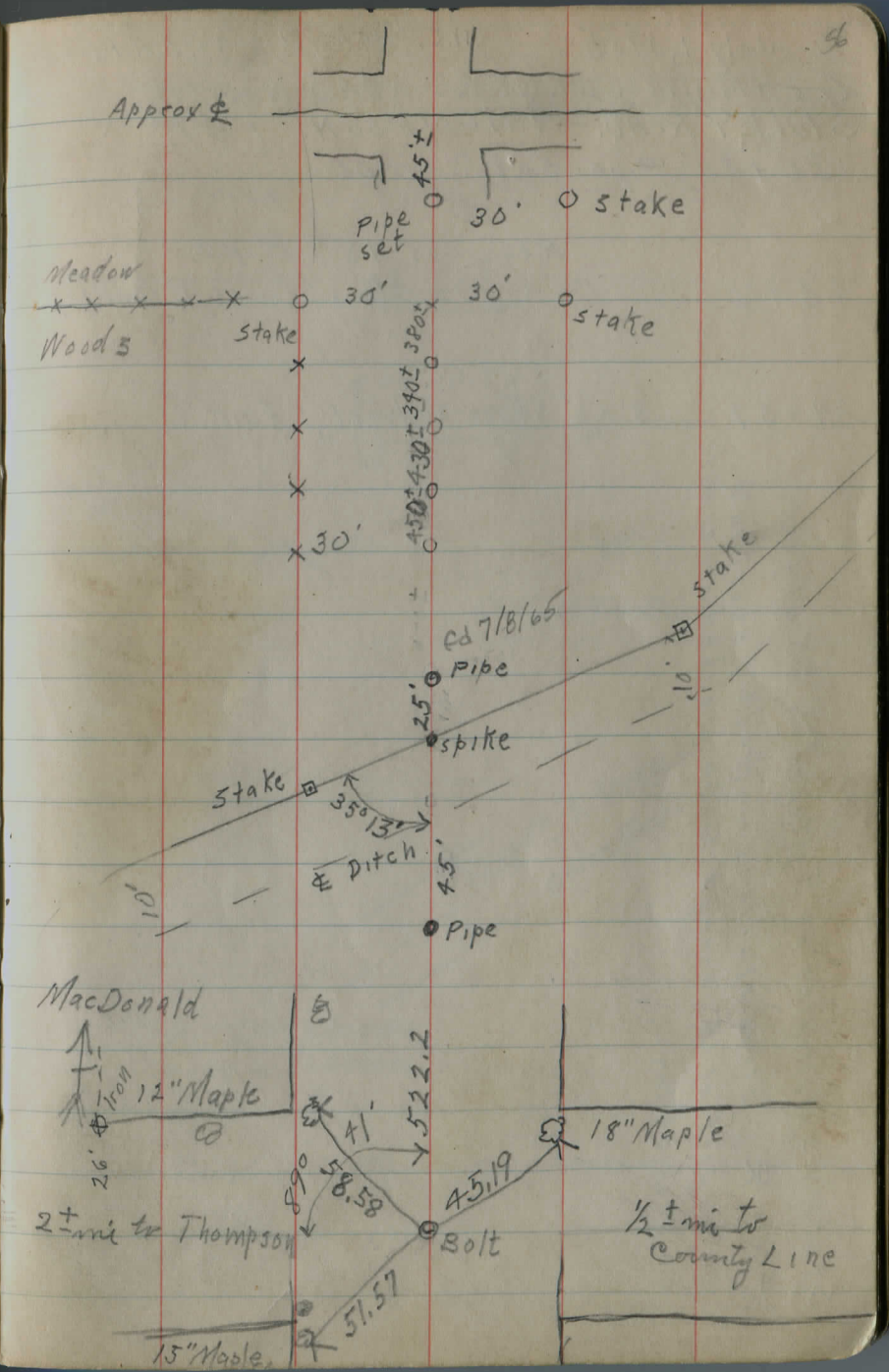
Stringers 7 - 3x10

Cuts from hubs

| | |
|---|---|
| Sta 0 | 3.61 |
| 1 | 2.72 |
| 2 | 2.50 |
| 3 | 3.59 |
| 4 | 3.02 |
| 5 | 3.36 |
| 6 | 2.43 |
| 7 | 2.34 |

13
7
10.5

GERMANY CORNERS NORTH.
THOMPSON TWP. T.H.59
W.C. Marks
June 14, 1935, Fair, 75°, Archie Alderman.
Sidley ROAD




Point set and referenced by F.R. Zethmayr in 1930, Survey of MacDonald Parcel

July 1, 1935 W.C. Marks, D. Parks, E.A. Parks

~~GERMANY CORNERS ROAD NORTH,~~
SIDLEY ROAD. — THOMPSON TWP.

30+00, Pipe Set, 0°00'

Requires 18" Pipe

28+10 1½'x1'/½' Stone Sluice Plank Tops

24+57 3'x2' Stone Culvert, fair

Stations, Multiples of 5, staked on 30' offset from ℄, other stations marked by short lath on offset of 15', except those marked otherwise on back of lath.



Meadow 32+89

Woods

~~Woods~~ 31+89 Woods

~~Woods~~

Woods

stake 30' Pipe Fd 7/8/65

2' 14'

5.4 11.1

Woods

21+72

Woods

15+80

5+51.5± ℄ bridge being Built. Stone Abuts., span 10'

Iron 24.2 meas

P.I. 25.0 Deed.

4+48.4

26.0' @ Iron

781.3

8 Post's

July 2, 1935

out

80+49.04 = 17°42' L

10" Tulip

70.0'

77+00, Δ=0°00'

Pipe

Revised
Defl + 0°15'

Fd 7/8/65

50.0

50.0

18" Gum?
Peppermidge?

Plank sluice 8" x 8"
Requires 15" Pipe

73+40

100 B.

66+55

150' H

66+05 P.L.

12" Cast Iron Pipe

65+05

P.L.? 58+50

57+57

H 100'±

57+17

44+82

50± H

44+35

fd 12-8-43
3-19-73

14" Pear

87.6

Twin 4" Evergreens

P.T.H. 49

43+43.37 ℄ E+W. Rd.

Δ = 0°14'30" L

Fd 7/8/65

Pipe set

68.0

11°45½'

5.0 Chs

90°10'

41.40

CEI # 57/5050

42+91.9 0°00' Pipe

Field

36+86

Woods

1.674 miles

5280 | 8840.5

July 3, 1935

88+55.0

Tacked stake

88+40.5

I.F. 48

Approx. ℄ County Line Road

90°45'±

88+21, 12" Corr. Pipe

28' long

P.C.T. out

84+00 Δ = 6°45" L

Stopped, July 2, 1935

8" oak clump

64.0

Pipe

50.1

N.W. root, 18" Maple

64.5

6" Maple

out

81+50 Δ = 4°00' R

Spike

80+82.55

6.71 6.71

6.74 6.74

width - 14

span - c.℄ height - 9'

I Beams, Plank Floor

Lattice Rails

Stone Abutments

Fair Condition.

80+61.07

80+49

July 3, 1935 W.C. Marks, E.A. Parks, D. Parks Fair, 85°

~~GERMANY CORNERS NORTH~~, THOMPSON

SIDLEY ROAD

| | | | | |
|---|---|---|---|---|
| B.M | 6.82 | 1043.18 | | 1036.36 |
| | 7.96 | 1048.32 | 2.82 | 1040.36 |
| 0-200 | | | 3.0 | 1045.3 |
| 0-100 | | | 4.2 | 1044.1 |
| 0+00 | | | 4.2 | 1044.1 |
| 0+14 | | | 4.6 | 1043.7 |
| 0+40 | | | 6.2 | 1042.1 |
| 1 | | | 8.2 | 1040.1 |
| 2 | | | 9.6 | 1038.7 |
| | 2.74 | 1043.10 | 7.96 | 1040.36 |
| 3 | | | 5.0 | 1038.1 |
| 4 | | | 5.0 | 1038.1 |
| 5 | | | 5.2 | 1037.9 |
| 5+51.5 | | | 10.6 | 1032.5 |
| 6 | | | 6.3 | 1036.8 |
| 7 | | | 6.4 | 1036.7 |
| | | | 6.76 | 1036.34 |
| B.M | 4.29 | 1040.65 | | 1036.36 |
| 8 | | | 4.0 | 1036.6 |
| 9 | | | 3.9 | 1036.7 |
| 10 | | | 4.5 | 1036.1 |



Spike, S.W Root, 30" Elm, 25' R. 7+15

| | | | | |
|---|---|---|---|---|
| 1041.6 | 1042.5 | 1044.1 | 1044.5 | 1045.1 |
| 6.7 | 5.8 | 4.2 | 3.8 | 3.2 |
| 200 | 100 | 0 | 100 | 200 |

5.2 8.7 6.3 — 6.1 7.4 5.2 5.5
30 24 17 14 — 17 20 24 30

5.3 9.2 8.2 — 8.5 9.3 6.8 5.9
30 23 15 13 — 10 13 18 30

10.2 9.6 10.3 9.9 — 10.1 10.6 9.6
30 11 9 8 — 12 14 17 30

5.3 — 5.0 6.3 5.3 4.1
25 15 — 13 15 17 30

6.9 5.8 5.2 — 5.2 6.6 6.0 5.4
30 11 9 — 12 17 18 30

6.5 6.2 5.2 — 5.6 6.3 6.5
25 7 3 — 10 13 30

Ditch Bottom

8.7 7.9 6.5 — 6.7 7.5
F 25 13 9 — 9 30

7.8 8.0 9.1 6.7 — 6.7 8.1 7.5 8.1
F 26 20 18-16 11 — 10 11-13 14 25

4.8 4.7 6.1 4.2 — 4.3 6.0 4.6
F 26 19 17-15 12 — 9 11-12 15 25

5.0 5.2 6.5 4.0 — 4.5 5.9 5.2 5.5
F 27 21 19 14 11 — 9 12-14 15 30

4.8 5.0 6.2 4.7 — 4.9 6.1 5.6 5.2 4.5
30 18 15 12 10 — 11 12-14 15 20 30

| | | | | |
|---|---|---|---|---|
| | | 1040.65 | | |
| 11 | | | 5.1 | 1035.5 |
| | | | | ~~1035.3~~ |
| 12 | | | 5.3 | 1035.3 |
| 13 | | | 5.2 | 1035.4 |
| | 5.25 | 1040.56 | 5.34 | 1035.31 |
| 14 | | | 4.6 | 1036.0 |
| 15 | | | 4.3 | 1036.3 |
| 16 | | | 4.9 | 1035.7 |
| 17 | | | 5.6 | 1035.0 |
| 18 | | | 6.2 | 1034.4 |
| 19 | | | 6.3 | 1034.3 |
| 20 | | | 6.6 | 1034.0 |
| | 5.18 | 1039.20 | 6.54 | 1034.02 |
| 21 | | | 5.4 | 1033.8 |
| 22 | | | 5.8 | 1033.4 |
| 23 | | | 5.9 | 1033.3 |
| 24 | | | 6.1 | 1033.1 |
| 24+57 | | | 5.0 | 1034.2 |



2.3/30 3.2/28 5.6/15 6.4/13 5.6/10 — 5.8/10 6.6/12 6.0/13 5.8/17 4.2/19 4.2/30

5.1/30 5.6/15 6.6/12 5.8/11 — 6.0/9 6.6/10 5.8/12 — 22 30

5.0/28 5.8/15 6.5/13 5.8/11 — 5.7/7 6.3/9 5.8/10 6.3/22-30

4.3/29 5.2/14 6.0/12 5.1/10 — 5.3/9 5.9/10 5.2/12 4.9/18 3.6/21-30

4.5/30 5.3/12 6.1/11 5.2/8 — 5.4/9 6.1/11 5.4/12 5.7/18 4.7/21-30

4.7/29 5.9/12 6.4/10 5.6/8 — 5.7/8 6.5/10 5.8/11 5.0/21-30

5.2/30 6.0/12 6.8/10 6.0/8 6.3/8 6.9/9 6.2/10 6.0/21-30

5.7/30 6.5/10 7.2/9 6.8/8 — 6.8/10 7.4/13 6.7/14 6.3/22-30

6.6/30 7.0/9 7.7/7 6.8/5 — 6.6/9 7.8/12 6.8/13 6.9/23-30

6.6/30 7.3/9 7.9/8 7.1/6 — 6.9/10 7.8/12 6.9/13-22-30

5.4/30 6.1/8 6.6/6 5.9/4 — 5.7/11 6.6/14 5.8/15-24-30

30-7 6.1/7 6.8/5 6.0/3 — 5.5/5 6.1/13 6.8/14 6.0/16 6.2/24-30

30 6.1/7 7.2/5 6.1/2 — 6.3/13 7.0/15 6.3/17 6.5/24-30

6.5/30 6.5/6 7.2/5 6.5/4 — 5.7/5 6.7/14 7.5/15 6.6/17 6.7/25-30

1032.9 1031.5

6.3/30 7.7 5.7-4.9/5.4 —

1031.7 1031.6 1031.3

5.1/11.1 6.1 7.5 7.6/100 7.9/200 Swamp

| | | | | |
|---|---|---|---|---|
| | | 1039.20 | | |
| 25 | | | 5.8 | 1033.4 |
| B.M. | | | 5.94 | 1033.26 |
| 26 | | | 5.7 | 1033.5 |
| | 5.18 | 1038.65 | 5.73 | 1033.47 |
| 27 | | | 5.3 | 1033.1 |
| 28 | | | 5.2 | 1033.4 |
| 28+10 | | | 5.0 | 1033.6 |
| 29 | | | 5.4 | 1033.2 |
| 30 | | | 5.0 | 1033.6 |
| | 6.73 | 1040.21 | 5.17 | 1033.48 |
| 31 | | | 6.3 | 1033.9 |
| 32 | | | 5.9 | 1034.3 |
| 33 | | | 5.2 | 1035.0 |
| 34 | | | 4.4 | 1035.8 |
| 35 | | | 3.1 | 1037.1 |
| | 7.90 | 1045.50 | 2.61 | 1037.60 |
| 36 | | | 7.7 | 1037.8 |
| 37 | | | 7.3 | 1038.2 |

$\frac{6.6}{30}$ $\frac{6.5}{6}$ $\frac{7.0}{5}$ $\frac{6.2}{2}$ — $\frac{6.1}{12}$ $\frac{7.1}{16}$ $\frac{6.5}{18}$ $\frac{6.7}{30}$

Spike, Westroot, 18" Maple, 25' right, Sta 24+80

$\frac{5.3}{30}$ $\frac{5.6}{13}$ $\frac{6.6}{10}$ $\frac{6.2}{6}$ $\frac{6.9}{4}$ $\frac{5.9}{2}$ — $\frac{6.0}{14}$ $\frac{7.2}{16}$ $\frac{6.4}{17}$ $\frac{6.0}{26}$

$\frac{5.5}{30}$ $\frac{5.6}{5}$ $\frac{6.5}{4}$ $\frac{5.6}{2}$ — $\frac{5.5}{15}$ $\frac{7.0}{17}$ $\frac{6.1}{19}$ $\frac{5.6}{30}$

$\frac{5.8}{30}$ $\frac{6.3}{5}$ — $\frac{5.3}{13}$ $\frac{7.0}{17}$ $\frac{6.3}{19}$ $\frac{6.5}{30}$

1031.8 1031.6 1031.6 1031.3

$\frac{5.8}{30}$ $\frac{6.8}{F.L.}$ $\frac{5.0}{2}$ $\frac{5.2}{14}$ $\frac{7.0}{F.L.}$ $\frac{7.0}{100}$ $\frac{7.3}{200}$

$\frac{5.5}{30}$ $\frac{5.9}{5}$ $\frac{6.8}{4}$ $\frac{5.9}{2}$ — $\frac{6.0}{14}$ $\frac{7.0}{17}$ $\frac{6.9}{18}$ $\frac{6.2}{30}$

$\frac{5.4}{30}$ $\frac{5.5}{8}$ $\frac{6.6}{7}$ $\frac{5.6}{5}$ — $\frac{5.7}{12}$ $\frac{7.0}{14}$ $\frac{6.0}{16}$ 30

Iron Pipe, ±, 30+06

$\frac{6.5}{30}$ $\frac{6.9}{8}$ $\frac{7.5}{6}$ $\frac{6.8}{4}$ — $\frac{7.1}{11}$ $\frac{7.8}{13}$ $\frac{7.3}{15}$ $\frac{6.7}{30}$

$\frac{6.4}{30}$ $\frac{6.5}{8}$ $\frac{7.3}{7}$ $\frac{6.3}{4}$ — $\frac{6.3}{11}$ $\frac{7.2}{13}$ $\frac{6.5}{15}$ $\frac{5.9}{30}$

$\frac{5.3}{30}$ $\frac{5.7}{7}$ $\frac{6.3}{5}$ $\frac{5.4}{3}$ — $\frac{5.7}{12}$ $\frac{6.2}{13}$ $\frac{5.5}{15}$ $\frac{5.0}{30}$

$\frac{4.5}{30}$ $\frac{3.5}{18}$ $\frac{4.5}{8}$ $\frac{5.4}{6}$ $\frac{4.6}{3}$ — $\frac{4.8}{11}$ $\frac{5.4}{13}$ $\frac{4.4}{15}$ $\frac{3.0}{30}$

$\frac{3.8}{30}$ $\frac{3.3}{8}$ $\frac{4.2}{6}$ $\frac{3.5}{4}$ — $\frac{3.1}{10}$ $\frac{3.7}{12}$ $\frac{2.8}{13}$ $\frac{2.3}{30}$

$\frac{8.5}{30}$ $\frac{8.1}{8}$ $\frac{8.8}{7}$ $\frac{8.1}{5}$ — $\frac{8.0}{9}$ $\frac{8.6}{11}$ $\frac{7.8}{12}$ $\frac{7.5}{30}$

$\frac{7.4}{30}$ $\frac{7.5}{8}$ $\frac{8.2}{6}$ $\frac{7.7}{4}$ — $\frac{7.5}{9}$ $\frac{8.2}{11}$ $\frac{7.4}{15}$ $\frac{7.4}{30}$

| | | | | |
|---|---|---|---|---|
| | | 1045.50 ✓ | | |
| 38 | | | 6.8 | 1038.7 |
| 39 | | | 5.9 | 1039.6 |
| 40 | | | 5.2 | 1040.3 |
| 41 | | | 4.6 | 1040.9 |
| 42 | | | 4.7 | 1040.8 |
| T.P. 42+91.9 | | | 5.62 | 1039.88 ✓ |
| July 5, 1935, W.C. Marks | | David + E.A } Parks | | 90° F. a.m. Storm at noon |
| | 4.28 | 1044.16 ✓ | | 1039.88 ✓ |
| 43 | | | 4.2 | 1040.0 |
| 43+43.37 | | | 4.8 | 1039.4 |
| 44 | | | 5.4 | 1038.8 |
| B.M. set | | | 4.40 | 1039.76 ✓ |
| 45 | | | 7.2 | 1037.0 |
| 46 | | | 9.3 | 1034.9 |
| 47 | | | 11.2 | 1033.0 ✓ |
| | | | 11.99 | 1032.17 |
| | 0.25 | 1032.42 ✓ | | |
| 48 | | | 1.4 | 1031.0 |
| 49 | | | 3.7 | 1028.7 |



$\frac{6.6}{30}\ \frac{6.9}{8}\ \frac{7.7}{6}\ \frac{7.1}{4}$ — $\frac{6.5}{5}\ \frac{6.9}{10}\ \frac{7.4}{13}\ \frac{6.7}{15}\ \frac{6.6}{30}$

$\frac{5.6}{30}\ \frac{6.1}{8}\ \frac{6.9}{7}\ \frac{6.2}{4}$ — $\frac{5.7}{5}\ \frac{6.0}{10}\ \frac{6.7}{12}\ \frac{5.9}{14-30}$

$\frac{4.6}{30}\ \frac{5.5}{10}\ \frac{6.1}{8}\ \frac{5.5}{4}$ — $\frac{5.4}{10}\ \frac{6.0}{11}\ \frac{5.2}{14-30}$

$\frac{4.3}{30}\ \frac{4.8}{10}\ \frac{5.7}{8}\ \frac{5.0}{6}$ — $\frac{4.8}{8}\ \frac{5.5}{10}\ \frac{4.6}{12}\ 30$

$\frac{4.3}{30}\ \frac{4.9}{12}\ \frac{5.8}{10}\ \frac{4.9}{7}$ — $\frac{5.0}{7}\ \frac{5.7}{10}\ \frac{4.4}{11}\ \frac{4.5}{30}$

Pipe on ℄

$\frac{3.7}{30}\ \frac{4.4}{16}\ \frac{5.0}{13}\ \frac{4.4}{11}$ — $\frac{4.9}{14}\ \frac{4.3}{30}$

1036.1 1038.9 1037.8 1034.7

$\frac{8.1}{200}\ \frac{5.3}{100}$ — $\frac{6.4}{100}\ \frac{10.0}{200}$

$\frac{4.7}{30}$ — $\frac{5.4}{10}\ \frac{5.8}{12}\ \frac{4.8}{13}\ \frac{4.6}{30}$

R.P. Spike, N.W. root, 24" Pear, 50' ± Right, Sta 44+15

$\frac{6.9}{30}\ \frac{7.0}{10}\ \frac{8.0}{8}\ \frac{7.4}{6}$ — $\frac{7.4}{7}\ \frac{8.1}{10}\ \frac{7.0}{12}\ \frac{6.5}{30}$

$\frac{9.0}{30}\ \frac{10.3}{12}\ \frac{9.6}{10}\ \frac{}{7}$ — $\frac{9.5}{5}\ \frac{10.2}{7}\ \frac{9.3}{9}\ 30$

$\frac{10.6}{30}\ \frac{11.2}{11}\ \frac{11.9}{9}\ \frac{11.3}{7}$ — $\frac{11.5}{6}\ \frac{12.0}{7}\ \frac{11.1}{10}\ \frac{10.5}{30}$

$\frac{0.7}{30}\ \frac{1.2}{10}\ \frac{2.6}{8}\ \frac{1.8}{5}$ — $\frac{1.6}{7}\ \frac{2.4}{10}\ \frac{1.5}{12}\ \frac{1.0}{20-30}$

$\frac{2.4}{30}\ \frac{3.0}{11}\ \frac{5.8}{8}\ \frac{4.0}{4}$ — $\frac{4.0}{7}\ \frac{5.0}{10}\ \frac{3.8}{11}\ \frac{3.2}{30}$

| | | | | |
|---|---|---|---|---|
| | | 1032.42 | | |
| 50 | | | 6.5 | 1025.9 |
| 51 | | | 9.5 | 1022.9 |
| 52 | | | 12.0 | 1020.4 |
| | 2.30 | 1022.27 | 12.45 | 1019.97 |
| 53 | | | 4.4 | 1017.9 |
| 54 | | | 6.9 | 1015.4 |
| 55 | | | 9.0 | 1013.3 |
| 56 | | | 11.2 | 1011.1 |
| | 0.48 | 1010.71 | 12.04 | 1010.23 |
| 57 | | | 2.4 | 1008.3 |
| 58 | | | 4.5 | 1006.2 |
| 59 | | | 6.0 | 1004.7 |
| 60 | | | 6.7 | 1004.0 |
| 61 | | | 8.1 | 1002.6 |
| | 0.32 | 1000.69 | 10.34 | 1000.37 |
| 62 | | | 1.3 | 999.4 |
| 63 | | | 4.5 | 996.2 |
| 64 | | | 5.7 | 995.0 |
| 65 | | | 6.8 | 993.9 |

65+30± Requires 18" Pipe

$\frac{5.5}{30}$ $\frac{6.1}{10}$ $\frac{7.5}{8}$ $\frac{7.0}{6}$ — $\frac{6.8}{7}$ $\frac{7.5}{9}$ $\frac{6.5}{10}$ $\frac{5.7}{30}$ $\frac{7.0}{6}$

$\frac{8.1}{30}$ $\frac{9.0}{10}$ $\frac{10.7}{8}$ $\frac{9.8}{5}$ — $\frac{9.6}{7}$ $\frac{10.6}{10}$ $\frac{9.4}{12}$ $\frac{8.7}{30}$

$\frac{10.9}{30}$ $\frac{11.2}{10}$ $\frac{13.3}{7}$ $\frac{12.4}{5}$ — $\frac{12.2}{7}$ $\frac{13.5}{10}$ $\frac{11.8}{12}$ $\frac{10.9}{30}$

$\frac{3.5}{30}$ $\frac{3.9}{9}$ $\frac{5.5}{7}$ $\frac{4.7}{4}$ — $\frac{4.7}{7}$ $\frac{5.6}{9}$ $\frac{3.7}{12}$ $\frac{3.3}{30}$

$\frac{5.8}{30}$ $\frac{6.7}{11}$ $\frac{8.8}{8}$ $\frac{7.5}{5}$ — $\frac{7.0}{8}$ $\frac{7.9}{11}$ $\frac{6.5}{14}$ $\frac{5.9}{30}$

$\frac{8.3}{30}$ $\frac{8.8}{11}$ $\frac{10.9}{8}$ $\frac{9.3}{3}$ — $\frac{9.3}{9}$ $\frac{10.2}{11}$ $\frac{8.9}{14}$ $\frac{9.1}{30}$

$\frac{11.1}{30}$ $\frac{11.1}{12}$ $\frac{13.2}{9}$ $\frac{11.7}{6}$ — $\frac{11.6}{8}$ $\frac{12.5}{11}$ $\frac{10.7}{13}$ $\frac{11.3}{30}$

$\frac{0.5}{30}$ $\frac{1.3}{12}$ $\frac{3.6}{9}$ $\frac{2.8}{6}$ — $\frac{2.7}{10}$ $\frac{4.0}{13}$ $\frac{0.1}{19}$ $\frac{0.5}{30}$

$\frac{4.3}{30}$ $\frac{4.4}{11}$ $\frac{5.4}{9}$ $\frac{4.4}{7}$ — $\frac{5.2}{10}$ $\frac{5.8}{12}$ $\frac{4.9}{14}$ $\frac{5.7}{30}$

$\frac{7.7}{30}$ $\frac{6.6}{9}$ $\frac{7.1}{8}$ — $\frac{6.1}{10}$ $\frac{6.8}{13}$ $\frac{6.1}{14}$ $\frac{7.1}{30}$

$\frac{6.9}{24}$ $\frac{7.4}{9}$ $\frac{8.3}{7}$ $\frac{7.4}{5}$ — $\frac{7.2}{9}$ $\frac{8.1}{12}$ $\frac{7.1}{14}$ $\frac{7.6}{30}$

$\frac{8.1}{23}$ $\frac{8.7}{11}$ $\frac{10.4}{8}$ $\frac{8.8}{5}$ — $\frac{8.8}{9}$ $\frac{10.6}{12}$ $\frac{6.0}{22}$ $\frac{6.7}{30}$

$\frac{3.0}{30}$ $\frac{0.8}{23}$ $\frac{1.5}{9}$ $\frac{3.5}{7}$ $\frac{1.7}{3}$ — $\frac{1.8}{7}$ $\frac{3.5}{10}$ $\frac{0.5}{15}$ $\frac{0.2}{30}$

$\frac{5.4}{24}$ $\frac{4.4}{9}$ $\frac{5.5}{6}$ $\frac{4.8}{4}$ — $\frac{4.7}{8}$ $\frac{5.4}{10}$ $\frac{3.6}{13}$ $\frac{2.3}{30}$

$\frac{6.7}{25}$ $\frac{5.9}{9}$ $\frac{6.7}{7}$ $\frac{6.0}{5}$ — $\frac{6.1}{8}$ $\frac{6.9}{10}$ $\frac{6.2}{11}$ $\frac{5.2}{30}$

$\frac{7.1}{24}$ $\frac{7.0}{8}$ $\frac{7.9}{7}$ $\frac{7.1}{5}$ — $\frac{7.1}{9}$ $\frac{8.0}{11}$ $\frac{6.9}{12}$ $\frac{5.9}{30}$

| | | | | |
|---|---|---|---|---|
| | | 1000.69 | | |
| 66 | | | 8.0 | 992.7 |
| 67 | | | 8.2 | 992.5 |
| | 4.75 | 997.04 | 8.40 | 992.29 |
| 68 | | | 4.4 | 992.6 |
| 69 | | | 3.4 | 993.6 |
| 70 | | | 4.5 | 992.5 |
| 71 | | | 6.8 | 990.0 |
| | 3.06 | 992.43 | 7.67 | 989.37 |
| 72 | | | 5.0 | 987.4 |
| +70 | | | 10.2 | 982.2 |
| 73 | | | 11.0 | 981.4 |
| +40 | | | 11.5 | 980.9 |
| 74 | | | 10.4 | 982.0 |
| | 7.79 | 994.30 | 5.91 | 986.51 |
| 75 | | | 6.7 | 987.6 |
| 76 | | | 4.8 | 989.5 |
| B.M set | | | 2.53 | 991.77 |
| 77 | | | 5.2 | 989.1 |
| 78 | | | 9.7 | 984.6 |



Gravel, Sta 58+40 to 67+50

989.5
11.2

creek 130

8.1 8.4 9.3 8.6 — 8.0 8.8 7.8 7.5
24 10 8 5 — 8 10 15 30

9.5 8.6 9.7 8.7 — 8.7 9.6 8.6 8.3 6.6
26 9 7 3 — 8 11 13 23 30

7.6 4.7 5.5 4.6 — 4.6 5.1 4.4 2.9
25 10 8 5 — 6 7 9 30

8.0 6.0 4.3 4.6 3.8 — 3.5 4.1 3.5 2.7
30 24 11 10 7 — 5 7 8 30

4.5 4.1 4.3 5.6 4.8 — 4.7 5.7 4.6 3.8
30 23 13 10 7 — 3 6 9 30

7.2 7.0 6.6 8.0 7.0 — 7.0 8.0 5.2 4.8
30 22 14 11 8 — 3 6 14 30
Rock

Spike, S.E. Root, 15" W, cherry, 20' Left, 71+60

7.0 5.1 4.0 6.1 5.1 — 5.3 6.0 1.4 1.0
30 22 12 9 7 — 5 6-8 19 30
Rock Ledge

14.3 14.3 11.3 — 11.2 12.0 2.6
30 16 9 — 4 6 24-30

11.9
14.5
30 14 10.8 7 — 10.9 8 3.5 3.0
20 30

16.0 5.8 5.4 7.8 7.2 — 7.1 7.5 6.6 5.4
30 17 12 8 5 — 10 12 14 30

5.1 5.3 6.1 5.1 — 5.0 5.9 4.8 4.1
25 11 9 7 — 5 8 10 30

R.P. Spike, S. side, 18" Gum?, 45' L. 76+90

4.3 4.6 6.0 5.0 — 6.4 5.1 4.3
30 18 14 11 — 3 6 30

5.0 5.0 10.0 9.7 — 10.2 5.0 4.9
30 25 11 11 — 4 14 30
Rock

| | | | | |
|---|---|---|---|---|
| | | 994.30 | | |
| | 6.81 | 789.24 | 11.87 | 982.43 |
| 79 | | | 10.8 | 978.4 |
| | -0.03 | 782.40 | 6.81 | 982.43 |
| 80 | | | 14.5 | 967.9 |
| T.P. | ~~9.73~~ | ~~972.45~~ | 15.78 | 966.62 |

July 6, Fair, 85°, W.C. Marks, D.R. Parks, E.A. Parks

| | | | | |
|---|---|---|---|---|
| T.P | 4.07 | 972.69 | | 966.62 |
| 80 | | | 4.8 | 967.9 |
| T.P. | 1.86 | 968.48 | | 966.62 |
| 80+49 | | | 4.0 | 964.5 |
| 81+00 | | | 4.8 | 963.7 |
| 80+61.1 | | | 4.5 | 964.0 |
| 80+82.6 | | | 4.8 | 963.7 |
| | | | 14.3 | |
| 80+72 | | | | 954.2 |
| 81+50 | | | 4.3 | 964.2 |
| T.P. | 3.80 | 970.42 | | 966.62 |
| 82 | | | 4.7 | 965.7 |
| +30 | | | 2.4 | 968.0 |
| | 14.38 | 984.72 | 0.08 | 970.34 |



$\frac{12.0}{50}$ $\frac{2.2}{35}$ $\frac{11.3}{8}$ $\frac{10.9}{7}$ — $\frac{11.2}{5}$ $\frac{2.2}{20}$ $\frac{2.9}{30}$

On South end, West Rail of Bridge

$\frac{15.6}{75-62}$ $\frac{14.1}{54}$ $\frac{12.8}{20}$ $\frac{3.7}{6}$ $\frac{4.6}{4}$ — $\frac{4.8}{8}$ $\frac{3.7}{11}$ $\frac{9.6}{20}$ $\frac{9.4}{30}$ $\frac{0.0}{45}$

Creek Bed

$\frac{11.0}{30}$ $\frac{10.5}{19}$ $\frac{4.3}{8}$ — $\frac{4.2}{4}$ $\frac{9.4}{15-30}$

$\frac{11.0}{30-17}$ $\frac{5.0}{7}$ — $\frac{4.9}{7}$ $\frac{10.7}{17}$ $\frac{11.0}{30}$

Stream Bed

$\frac{5.0}{30}$ $\frac{8.8}{24-9}$ — $\frac{4.1}{12}$ $\frac{11.0}{25}$ $\frac{12.3}{30}$

953.4

$\frac{0.0}{29}$ $\frac{7.2}{23}$ $\frac{4.2}{17}$ $\frac{}{12}$ — $\frac{4.7}{4}$ $\frac{11.7}{12}$ $\frac{17.0}{30}$ water Level

+16± Top of 45 B. Bank $\frac{+10.5}{30}$ $\frac{1.4}{16}$ $\frac{0.6}{12}$ $\frac{2.0}{9}$ — $\frac{2.4}{3}$ $\frac{18.2}{20-30}$ creek bed

| | | | | |
|---|---|---|---|---|
| | | 984.72 ✓ | | |
| 83 | | | 7.1 | 977.6 ✓ |
| | 11.79 | 993.90 ✓ | 2.61 | 982.11 ✓ |
| B.M. | | | 4.91 | 988.99 |
| 84 | | | 8.2 | 985.7 |
| 85 | | | 5.6 | 988.3 |
| 86 | | | 4.2 | 989.7 |
| 87 | | | 4.2 | 989.7 |
| 88 | | | 4.4 | 989.5 |
| 88+40.5 | | | 4.7 | 989.2 |

+4.5 / 30-18 — 0.0 / 14 — 7.6 / 4 (Rock) — 6.6 / 10 — 7.3 / 12 — 5.8 / 15 — 32.5 / 40'± Bank to Creek

R.P. Spike, N.W. root, 18" Maple, 45'± Right 83+70

4.3 / 30-13 — 9.4 / 9 — 8.4 / 7 — 8.2 / 4 — 9.2 / 6 — 4.7 / 15-30

3.8 / 30 — 4.4 / 16 — 7.0 / 11 — 6.0 / 8 — 5.6 / 3 — 6.5 / 5 — 5.0 / 8 — 4.7 / 36

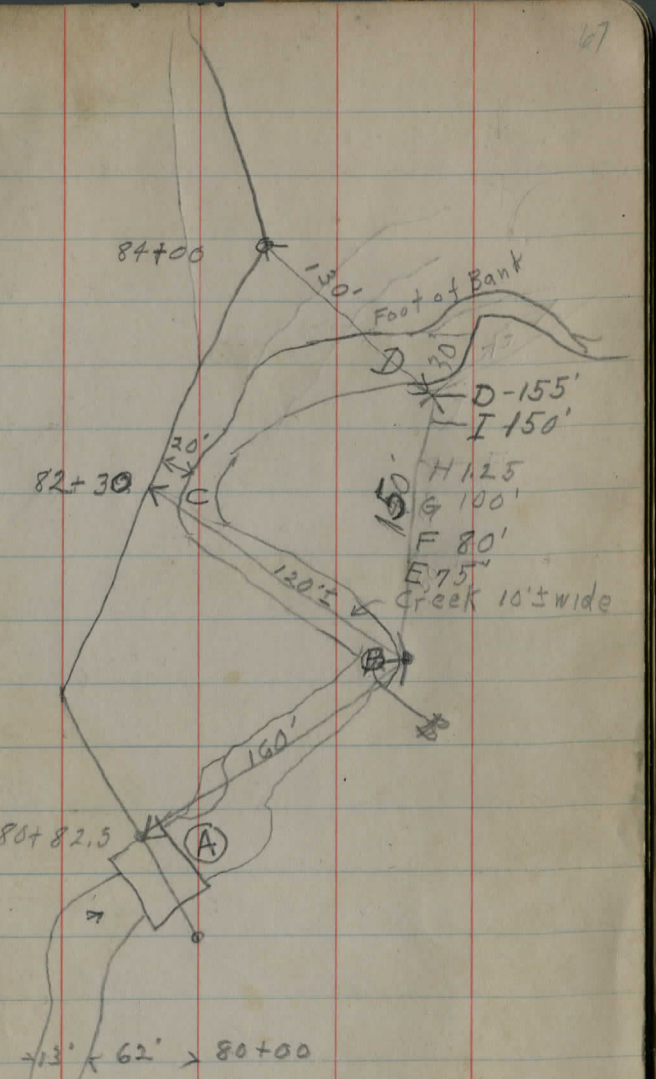
3.9 / 30 — 4.8 / 13 — 5.6 / 10 — 4.5 / 8 — 4.5 / 4 — 5.5 / 8 — 4.8 / 9 — 5.1 / 30

3.8 / 30 — 4.7 / 12 — 5.6 / 11 — 4.6 / 6 — 4.6 / 6 — 5.5 / 8 — 4.7 / 9 — 4.9 / 30

4.6 / 30 — 5.0 / 11 — 5.7 / 9 — 4.7 / 6 — 4.9 / 6 — 6.0 / 9 — 5.4 / 10 — 5.5 / 30

992.0 / 1.9 / 200 — 990.5 / 3.4 / 100 — 987.9 / 6.0 / 100 — 985.9 / 8.0 / 200

| | | | | |
|---|---|---|---|---|
| T.P. | -6.81 | 959.81 | | 966.62 |
| Point A | | | 6.2 | 953.6 |
| B | | | 6.6 | 953.2 |
| C | | | 7.6 | 952.2 |
| E | | | 5.1 | 954.7 |
| F | | | 8.1 | 951.7 |
| G | | | 7.9 | 951.9 |
| H | | | 7.3 | 952.5 |
| I | | | 8.7 | 951.1 |
| D | | | 10.7 | 949.1 |



Pg. 69 + 70

Ripped out

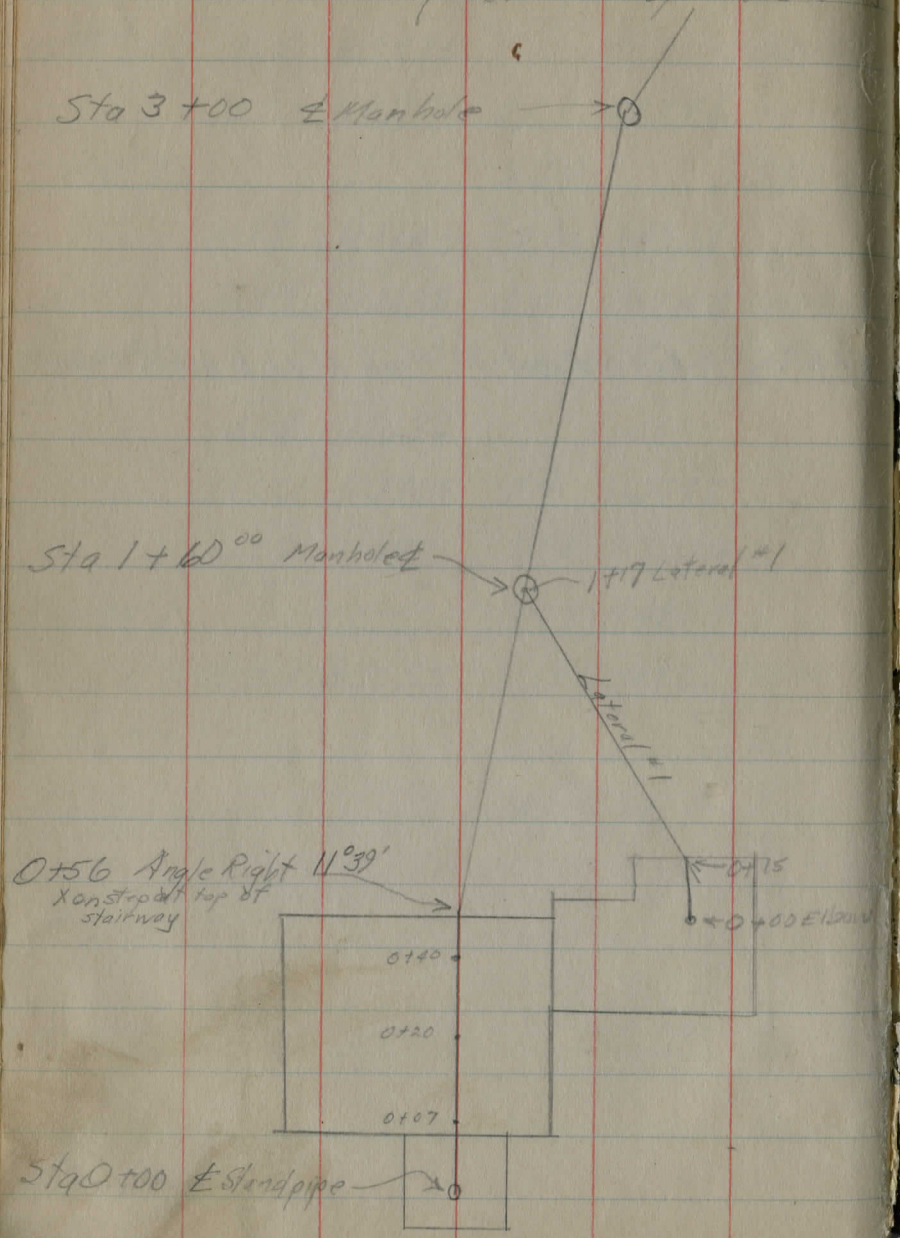
| | | | | | |
|---|---|---|---|---|---|
| | BM Level Mosley Road | | | | |
| BM #10 | 2.68 | 1093.71 | | | 1090.03 |
| | 9.73 | 1102.19 | 0.25 | 1093.46 | ~~1102.63~~ |
| BM #9 | | | 6.50 | | 1102.63 |
| | 11.87 | 1121.05 | 0.01 | 1109.18 | |
| BM | 7.33 | 1126.38 | 2.00 | 1119.05 | ~~1122.32~~ |
| BM #8 | | | 4.06 | 4.04 | 1122.32 |
| | 4.04 | 1126.36 | | | |
| | 12.26 | 1137.08 | 1.54 | 1124.82 | |
| | 11.77 | 1148.81 | 0.04 | 1137.04 | |
| Cut-Off #1 | | | 8.58 | 1140.23 | |
| | 6.94 | N55.55 | 1.20 | 1148.61 | |
| BM #7 | | | 3.40 | | 1152.15 |
| | | | 4.19 | 51.36 | |

N.6.

N.6.

V.07 Nail N Edge of 30" Maple 25' Lt & 600 N Mosley Rd

Location Sanitary Sewer Pipe Residence



Sidestakes set 6' North

Sanitary Sewer Grades

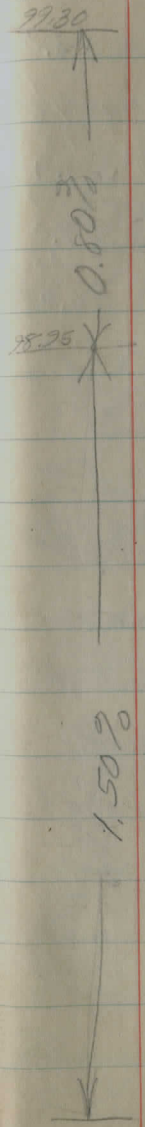
| | | | | Pipe | Residence |
|---|---|---|---|---|---|
| Old Floor | 4.60 | 104.60 | | 100.00 | |
| Bottom Trench | | | 5.27 | 99.33 | |
| Grade 0+00 | | | 5.30 | 99.30 | |
| 0+07 | | | 5.34 | 99.26 | C 1.0 |
| 0+20 | | | 5.46 | 99.14 | C 1.0 |
| 0+40 | | | 5.54 | 99.06 | C 1.0 |
| | 3.56 | 107.44 | 0.72 | 103.88 | |
| 0+56 | | | 8.49 | 98.95 | C 6.12 (2.37) |
| 0+75 | | | 18.77 | 98.67 | C 7.5 (1.27) |
| 1+00 | | | 9.15 | 98.29 | C 7.0 (2.15) |
| 1+25 | | | 9.52 | 97.92 | C 7.5 (2.02) |
| 1+50 | | | 9.90 | 97.54 | C 5.5 (4.40) |
| 1+60 | Manhole | | | 97.39 | |
| 1+75 | | | 10.27 | 97.17 | C 5.0 (5.27) |
| 2+00 | | | 10.65 | 96.79 | C 5.5 (5.16) |
| 2+25 | | | 11.02 | 96.42 | C 6.0 (5.02) |
| 2+50 | | | 11.40 | 96.04 | C 6.0 (5.40) |
| 2+75 | | | 11.77 | 95.67 | C 6.0 (5.77) |
| 3+00 | | | 12.15 | 95.29 | C 5.0 (7.15) |

3/21/39

74

Main Ditch

100 = Elev. Basement floor near Well



Stakes are set 6' South

Sanitary Sewer Grades, Pipe Residance

Lateral to New basement

| | | | | |
|---|---|---|---|---|
| | 3.76 | 102.64 | 103.88 | |
| 0+00 | 9' | 9.00 | 98.64 | |
| 0+15 | | 9.16 | 98.48 | C 2.0 |
| 0+50 | | 9.54 | 98.10 | C 7.6 |
| 0+75 | | 9.80 | 9784 | C 8.0 |
| 1+50 | | 10.07 | 97.57 | C 7.0 |
| 1+17 = 140 Main 07.6 | | 10.25 | 9739 | C 6.0 |

8.65

107
15
4.35
102
10

864
739
125 | 1.07
117
800

9864
54
9810
26
9784
27
9757

53
2'

117

107
17
749
67
82

51
18
3



Memmo. "Jug St." Troy Tpe
Vol. C, P. 30 / Beg. S. line Tp. a
little west of cent. of sec. #6, N. 1°-30' E
4 mi + 6 chains to the E. + W. road
near Beals saw mill. Thence N.
49° E, 12.25 ch. along the banks
of the mill pond to a post. Thence
N. 1°30' E 91.75 ch to the N. line of P.
N. 3 5° E. 5-4. ch to post standing in
E. line of Stull lot. Thence N. 1°-30'
E along said line 51. chains
to the intersection of the Co. road
leading from Parkman to Burton
whole distance 6 miles + 56 chs.
March 15th 1832

Vol. B. 402-3 x + 76. ch. to Beals
saw mill. Thence S. 77° W. 5 ch. to post
Thence N. 73° W 53. chs. till it intersects
the S. line of the G. Tkey lot so called
Thence W. along the same 16 ch. to the
to the E. + W. road to cent. Welch field —

Chil. Rd
Bridge

4/21-27 T. & F. Rec
— Rain —

New line to intersect ang. N. of bridge

23+63 - about 25' W. of S. end of bridge in ℄ Chi

2 0 near Prop. line
19+10 ℄ Chillicothe Rd.

ang. near N. end of Lane abt 11 ±0 +50.

9 about 5' E of large Boulder (BM)
8 near fence line
5 S. of Hen Park
4 near barn

Sta 0
Tel. pole ⊙ ⊙ South Trees of row E. side Chillicothe Rd

4/21-27 — Fiddes x Fiddes —

2363 X⁵ line at 5+00 (19+10)

8+80 ang to Left

10+50 " " Right

15. " " L x prof line

22+80

Preliminary new location

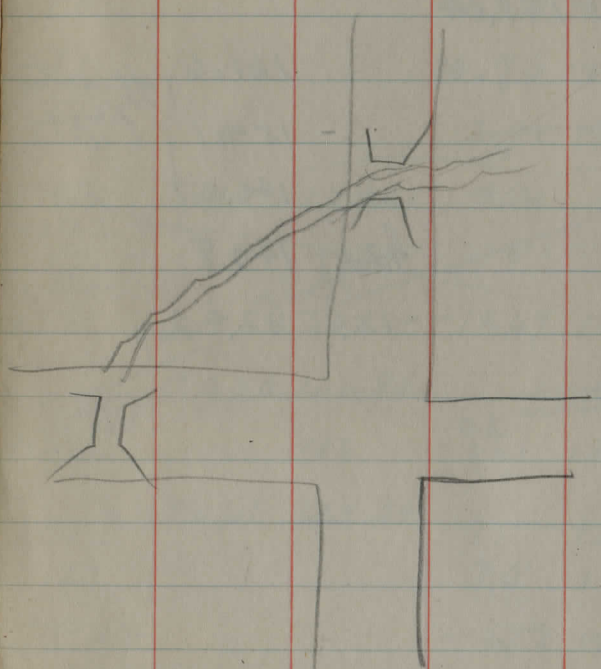
| | | | | | |
|---|---|---|---|---|---|
| | +1,03 | 201,03 | | 200,00 | azimuth & bet. bottom of cur. board S.E. cor. dwelling |
| 0 = 2 | | | 2,90 | 198.1 | |
| 1 | | | 3.50 | 197,5 | |
| 2 | | | 3,50 | 197.5 | |
| 3 | | | 4.30 | 196,7 | |
| 4 | | | 5,30 | 195.7 | near drive. |
| 5 | | | 8,30 | 192.7 | Near Prof S. fence |
| 6 | | | 12,30 | 188 7 x 190 | |
| Prop. T.P. | -12.00 | | -12,00 | 189,03 | |
| | +0.58 | 189.61 | | | |
| 7 | | | 8,50 | 181,1 | 182. |
| 8 | | | 17.00 | 172.6 | 174 |
| By T.P. | +1,10 | 177,99 | -12.92 | 176.69 | |
| Highest point G.M. | | | 12.50 | 165.3 | 166. |
| | | | -8.89 | 168,90 | Top of Boulder L.(W.) of 8 (2.9 Highest point) |

4/23 – 27 F. & S. Snowing

| Sta | +R | H.I. | -R | Elev. | Rem |
|---|---|---|---|---|---|
| B.M. | +0.10 | 169.00 | | 168.90 | |
| 9+50 stone | | | 7.40 | 161.6 | Ledge Rock |
| T.P. | | 169.00 | -12.57 | 156.43 | |
| | +0.46 | 156.89 | | | |
| 10 | | | 2.80 | 154.1 | |
| 11 stone T.P. | | | 10.70 | 146.2 | |
| | | | ~~-12.95~~ | ~~144.14~~ | |
| 12 100 to L stone T.P. | +0.13 | 144.27 | 4.20 | | |
| | | | 1.5 | | |
| | | | -12.67 | 131.60 | |
| | +0.30 | 131.90 | | | |
| R.T.P. Rock | | 133 | O.K. -12.61 | 132.43 | |
| | +0.61 | 133.04 | | | |
| 30' to L 13 | | | 0.0 7.0 | 133 126.0 | |
| T.P. rock | | | -12.53 | 120.51 | |
| | +0.90 | 121.41 | | | |
| 40' to L 14 | | | 0.0 5.50 | 121.4 115.6 | |
| | | | -12.11 | 109.30 | |
| | +1.25 | 110.55 | | | |
| 15 | | | 2.90 | 107.7 | |



| Sta | +R | H.I. | -R | Elev. | |
|---|---|---|---|---|---|
| BM | +0.35 | 169.25 | | 168.90 | |
| | | | -12.60 | 156.65 | |
| | +0.72 | 157.37 | | | |
| | | | -12.58 | 144.79 | |
| | +0.25 | 145.04 | | | |
| 9+50 | | | | 161.6 | offsite ledge |
| 10 | | | - | 154.1 | |
| 11 | | | | 146.2 | |
| 12 | | | 4.2 | 140.8 | |
| | | | -12.61 | 132.43 | |



Culvert 800' N of school 1/2 mi E
of Thompson 3x2 stone box
[illegible] center top can be eliminated

| Sta | + Rod | H.I. | Rod | Elev | |
|---|---|---|---|---|---|
| 16 | | 110.58 | 7.80 | 102.8 | |
| 16+10 | | | 8.9 | 101.7 | |
| +40 apx | | | 19. | 91.6 = approx | |
| 16+75 | | | 10.0 | 100.6 | & gulley |
| 17 | | | 10.4 | 100.2 | |
| 18 | | | 11.7 | 98.9 | |
| Stake T.P. | | | -11.29 | 99.29 | |
| | +0.35 | 99.64 | | | |
| 18+85 | | | 7.0 | 92.6 | Tp. bank |
| | | | | 85.6 | |
| 18+90 | | | 11.0 | | |
| 19 | | | 10.6 | 89.0 | |
| +10 Ł ditch | | | 11.0 | 88.6 | |
| +20 | | | 14.5 | 85.1 | |
| Tp bank +35 | | | 9.0 | 90.6 | |
| 20 | | | 12.6 | 87.0 | |
| To R. Iron pipe at prop. line | | | -12.59 | 87.05 | 20 50 R20 |
| | +0.40 | 87.45 | | | |
| 21 | | | 7.7 | 79.7 | |
| +20 | | | 11.7 | 75.7 | |
| Pin TP | | | -12.25 | 75.20 | |

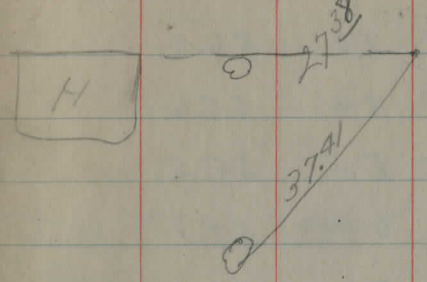
Smooth spindle

| | | H.I. | | Elev | |
|---|---|---|---|---|---|
| Pin | +0.22 | 75.42 | | 75.20 | |
| TP | | | -12.39 | 63.03 | |
| | +1.02 | 64.05 | | | |
| 21+75 | | | 8.0 | 56.0 | |
| 22 | | | 8.4 | 55.6 | |
| +10 | | | 8.5 | 55.5 | |
| +13 | | | 6.9 | 57.1 | Street Intersec |
| +28 | | | 7.0 | 57.0 | |
| +30 | | | 9.0 | 55.0 | |
| 23 | | | 9.5 | 54.5 | |
| +60 | | | 10.5 | 53.5 | Water 51.80 |
| +75 | ground | | 13.00 | 51.0 | Creek |
| S. Wear. & wrote Abut. & side | | Bridge | | Plum edge | |
| B.M. | | | -5.41 | 5864 | |
| & bridge S. side on plank | | | 3.85 | 60.20 | |

198.1
60.2
137.9

8% Sta. 6 to 14+50

7 1/2% " 22+50 " " " "




15
86
90
170

29 | 19000 | 1074
27
200
189
110
108

134

Harrison Road
Gardner

1150.98
12.00
1163.42
11.65
75.07
12.89
87.96
1.72
86.24
6.49
92.73